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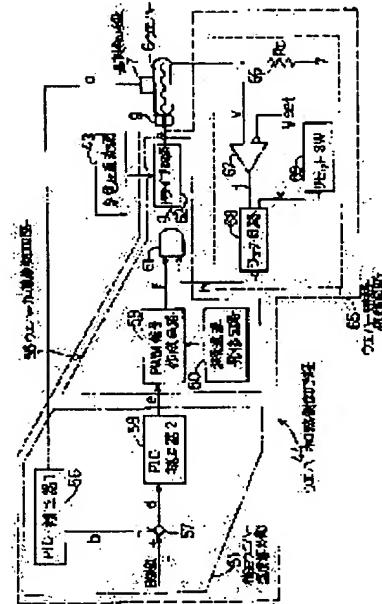
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(54) STERILE BONDING DEVICE FOR FLEXIBLE TUBE

(57)Abstract:

PURPOSE: To reduce consumed power, and allow the temperature control of a wafer by controlling a constant voltage source for heating the wafer for fusing and cutting a flexible tube on the basis of the detected temperature of the wafer.

CONSTITUTION: A wafer heating control means 44 has a deviation signal output part 57 for outputting a deviation signal (d) between a corrected temperature (b) calculated by the PID corrector 56 of a corrected wafer temperature calculating part 51 on the basis of the output (a) of a temperature detecting means 7 and a target heating temperature (c) of a wafer, and outputs a corrected deviation signal (e) by a PID corrector 58. Pulse width modulation signal output parts 59, 60 output a pulse width modulation signal (f) on the basis of the corrected deviation signal (e). Further, the wafer heating control means 44 has a drive circuit 62 for controlling a constant voltage source 43 by the pulse width modulation signal (f) and a pulse width modulation signal control part 61 for controlling the inflow of the pulse width modulation signal (f) from the pulse width modulation signal output part 59 to the drive circuit 62 on the basis of the detection signal (h) of the wafer short-circuit detecting parts 67, 58 of a wafer short-circuit protecting circuit 65.



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CLAIMS

[Claim(s)]

[Claim 1] It is equipment for joining a flexible tube in sterile. This equipment The 1st clamp and the 2nd clamp which hold at least two flexible tubes in the parallel condition, The cutting means for cutting said flexible tube between this 1st clamp and the 2nd clamp, It has the migration means to which either [at least] said 1st clamp or said 2nd clamp is moved so that both the edges to which the flexible tube cut by this cutting means is joined may stick. A wafer for said cutting means to carry out melting cutting of said flexible tube, It has the source of a constant voltage, wafer temperature detection means, and wafer heating control means for heating this wafer. Said wafer heating control means Flexible tube sterile junction equipment characterized by being what has the Pulse-Density-Modulation signal output part computed based on the output of said wafer temperature detection means, and controls said source of a constant voltage by this Pulse-Density-Modulation signal.

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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Industrial Application] This invention carries out heating fusion of at least two flexible tubes, and relates to the flexible tube sterile junction equipment for connecting in sterile.

[0002]

[Description of the Prior Art] At the time of tube connection of the blood collecting bag in a transfusion system and a constituent-of-blood bag, and exchange of the dialysing fluid bag in continuous ambulatory PD (CAPD), and a waste fluid bag, it is necessary to connect a tube in sterile. As equipment which makes sterile connection of such a tube, it is shown in JP,61-30582,B and there is a thing. The equipment shown in this JP,61-30582,B The 1st clamp and the 2nd clamp which are the tube contact which carries out heating fusion of the tube and is connected, and hold two flexible tubes which should be connected in the parallel condition, It has the cutting means for cutting a flexible tube between the 1st clamp and the 2nd clamp, and the migration means to which either [at least] the 1st clamp or the 2nd clamp is moved so that both the edges to which the flexible tube cut by the cutting means is joined may stick.

[0003] And the cutting means has the wafer for carrying out melting cutting of the flexible tube, and the power source for heating a wafer. As a power source for heating a wafer, the constant current source is used as shown in JP,59-64034,A. And the approach of predicting the temperature of a wafer from resistance is used for the temperature control of a wafer using the resistance temperature change of a resistor.

[0004]

[Problem(s) to be Solved by the Invention] However, by the approach the temperature control of a wafer predicts the temperature of a wafer from resistance using the resistance temperature change of a resistor using a constant current source, it actually has the trouble that it is difficult to perform positive temperature control since the temperature of a wafer is measured and it does not control as shown in JP,59-64034,A. furthermore, in the heating circuit using a constant current source, since loss of a drive circuit was large, it may be easy to be large [power consumption] and the trouble also had it. Then, the purpose of this invention can perform certainly temperature control of a wafer for heating melting to cut a flexible tube, and offers flexible tube sterile junction equipment with little power consumption further.

[0005]

[Means for Solving the Problem] It is equipment for joining a flexible tube in sterile which attains the above-mentioned purpose. This equipment The 1st clamp and the 2nd clamp which hold at least two flexible tubes in the parallel condition, The cutting means for cutting said flexible tube between this 1st clamp and the 2nd clamp, It has the migration means to which either [at least] said 1st clamp or said 2nd clamp is moved so that both the edges to which the flexible tube cut by this cutting means is joined may stick. A wafer for said cutting means to carry out melting cutting of said flexible tube, It has the source of a constant voltage, wafer temperature detection means, and wafer heating control means for heating this wafer. Said wafer heating control means It is flexible tube sterile junction equipment which is what has the Pulse-Density-Modulation signal output part computed based on the output of said wafer temperature detection means, and controls said source of a constant voltage by this Pulse-Density-Modulation signal.

[0006] And said wafer heating control means has the deflection signal output part which outputs the deflection signal of the amendment wafer temperature calculation section, the amendment temperature computed by this calculation section, and whenever [purpose stoving temperature / of said wafer] based on the output of said wafer temperature detection means, and, as for said Pulse-Density-Modulation signal output part, it is desirable that it is what outputs a Pulse-Density-Modulation signal based on this deflection signal. Furthermore, as for said wafer heating control means, it is desirable to have the wafer short circuit

protection network. Moreover, said wafer heating control means has the drive circuit for controlling said source of a constant voltage by this pulse-width-modulation signal, and, as for said wafer short circuit protection network, it is desirable to have the short circuit detection section of said wafer and the pulse-width-modulation signal-control section which controls an inflow in said drive circuit of the pulse-width-modulation signal from said pulse-width-modulation signal output part based on the detection signal of this short circuit detection section. Moreover, as for said amendment wafer temperature calculation section, it is desirable to have proportionality, the integral, and the differential correction circuit. Furthermore, as for said deflection signal output part, it is desirable to have proportionality, the integral, and the differential correction circuit. And as for said wafer temperature detection means, it is desirable that they are a thermocouple or a resistance bulb. Furthermore, as for said wafer temperature detection means, it is desirable that they are a sheath form thermocouple or a resistance bulb.

[0007] Then, the flexible tube sterile junction equipment of this invention is explained with reference to a drawing. The 1st clamp 3 and the 2nd clamp 2 which this flexible tube sterile junction equipment 1 is equipment for joining a flexible tube in sterile, and hold at least two flexible tubes in the parallel condition, The cutting means 5 for cutting the flexible tubes 48 and 49 between the 1st clamp 3 and the 2nd clamp 2, It has the migration means to which either [at least] the 1st clamp 3 or the 2nd clamp 2 is moved so that both edges 48a to which the flexible tubes 48 and 49 cut by the cutting means 5 are joined, and 49a may stick. The wafer 6 for the cutting means 5 to carry out melting cutting of the flexible tubes 48 and 49, It has the source 43 of a constant voltage, the wafer temperature detection means 7, and the wafer heating control means 44 for heating a wafer 6. The wafer heating control means 44 Based on the output of the wafer temperature detection means 7, it has the Pulse-Density-Modulation signal output part 59 computed, and the source 43 of a constant voltage is controlled by the Pulse-Density-Modulation signal.

[0008] Drawing 1 is the perspective view of one example of the flexible tube sterile junction equipment of this invention, drawing 2 is the perspective view showing the condition contained in the case the sterile junction equipment shown in drawing 1 , drawing 3 is the block diagram showing an example of the electrical circuit used for the sterile junction equipment of this invention, and drawing 4 is the electrical circuit block diagram showing an example of the wafer heating control means of the electrical circuit of the sterile junction equipment of this invention. Drawing 5 is the plan of one example of the flexible tube sterile junction equipment of this invention.

[0009] Next, the wafer heating control means indicated to drawing 4 is explained. What has the metal plate bent as a wafer 6 so that it might face each other, the insulating layer formed in the inside of this metal plate, the resistor formed so that the above-mentioned metal plate might not be contacted in this insulating layer, and the terminal for energization prepared in the both ends of this resistor is used suitably. And since a resistor generates heat by energization, generation of heat of a resistor is conducted to a metal plate, and the whole wafer generates heat by energization. And resistance changes with generation of heat according [a resistor] to energization. Therefore, the source of a constant voltage is only used and temperature control of enough wafers cannot be performed only by adjusting the electric power supply to a wafer. So, with the sterile junction equipment 1 of this example, it has the wafer heating control means.

[0010] As shown in drawing 4 , as for the wafer heating control means 44, it is desirable to have the wafer heating control circuit 55 and the amendment wafer temperature calculation circuit 51, and to have the wafer short circuit protection network 65 further, as shown in drawing 4 . The wafer heating control circuit 55 has the Pulse-Density-Modulation signal output part 59 computed based on the output of ** from the temperature detection means 7, and controls the source 43 of a constant voltage by the Pulse-Density-Modulation signal. Having the deflection signal output part 57 which outputs the deflection signal of the amendment temperature specifically computed by the amendment wafer temperature calculation section 56 which computes amendment wafer temperature, and the calculation section based on the output of the wafer temperature detection means 7, and whenever [purpose stoving temperature / of a wafer], the Pulse-Density-Modulation signal output part 59 outputs a Pulse-Density-Modulation signal based on a deflection signal. As a temperature detection means 7, it is desirable that they are a thermocouple or a resistance bulb. More preferably, it is a sheath form thermocouple or a resistance bulb, and a sheath form thermocouple is desirable especially.

[0011] If the heating control means 44 is more concretely explained using drawing 4 , the temperature detection signal a from the thermocouple which is the temperature detection means 7 will be inputted into the PID amendment machine 1 (proportionality and differential / integral amendment machine 1) which is the amendment wafer temperature calculation section 56, and the amended amendment temperature signal b will be outputted. With this PID amendment machine 56, it is formula $1b=1/-K-a-(1+K1 \text{ and } T-da/dt)$, for

example... (1)

It is alike and correction value is computed more. K is the coupling coefficient of a wafer and a thermocouple, K1 is a correction factor resulting from the flexible tube cut, and T is the thermal time constant of a thermocouple. The purpose which performs such amendment is to perform [performing amendment (K) based on the heat-conduction loss between a wafer and a thermocouple, and] amendment in consideration of the thermal time constant (T) of a thermocouple. And as shown in a formula 1, the amendment temperature signals $1/K$ are highly computed by K1 and $T \cdot da/dt$, while wafer temperature is rising from the surveyed wafer temperature signal a, since b is a constant. The temperature which a thermocouple detects is the internal temperature of a thermocouple, and has delay to the skin temperature of a wafer. However, since the delay of a thermocouple is approximated to first-order lag, it considers as a time constant T and the secondary progress operation of a time constant T is conversely performed as a correction function by performing the above-mentioned amendment, wafer skin temperature is correctly [without a time lag] computable.

[0012] Moreover, exact wafer skin temperature is correctly [without a time lag] computable by performing amendment as shown in a formula 1 also at the time of wafer temperature descent. And it will become a formula 2 if a formula 1 is rewritten in consideration of a sampling time ($**t$).

$$b(t+**t) = 1 - K \cdot a(t+**t) - \{1 + K1 \cdot T / **t - [a(t+**t) - a(t)]\} \dots (2)$$

Thus, the amendment temperature signal b computed is compared with the target wafer temperature signal c, and the deflection signal d is outputted by the deflection signal output part 57. This deflection signal d is inputted into the PID amendment machine 2 designed by the suitable transfer function in order to raise the responsibility of a control system, and it is outputted as an amendment deflection signal e. This amendment deflection signal e is inputted into the PWM (Pulse Density Modulation) signal creation circuit 59. The PWM signal creation circuit 59 synchronizes with the predetermined frequency created by the above-mentioned amendment deflection signal e and the above-mentioned subcarrier oscillator circuit 60, and outputs the signal (pulse train signal which carried out the PWM modulation) f of the pulse width proportional to the amendment deflection signal e. This pulse train signal f passes along a gate circuit 61, and flows into the drive circuit 62. The drive circuit 62 is constituted by a transistor, a thyristor, etc. which are a solid-state-switching component, inputted pulse train signal g acts as switching and a timing signal, and only when pulse train signal g is in the condition of H, the source of a constant voltage and a wafer are connected. Connection between the drive circuit 62 and a wafer 6 is made with the connection terminal 9. The source 43 of a constant voltage and a wafer 6 are intermittently connected based on pulse train signal g, and a wafer is controlled by the wafer temperature made into the purpose.

[0013] And when the outline of the heating circuit in the case of constant-current system comes to be shown in drawing 19 and loss of the heating circuit of constant-current system is searched for, loss (Wo) is $Wo' = (Vi - Vo) Io$ and is $Wo' = [Vce + \{(Vi - Vce) - Vo\}] Io$. It is set to (A). Moreover, the outline of the heating circuit in the case of PWM comes to be shown in drawing 20, and loss (Wo) of a drive circuit is $Wo = Vo/Vi - Vce - Io + W1$ (B),

W1 is the switching loss of the transistor which constitutes a drive circuit. And generally a comparison of Wo and Wo' materializes the following relation in B type.

Generally in $Vo/Vi - Vce - Io > W1$, next A type, the following relation is realized.

$Vce << (Vi - Vce) - Vo$ -- if this compares the 1st item of A type and B type, and the 2nd item -- $Vo/Vi - Vce - Io < Vce - Io$ $W1 < (Vi - Vce) - Vo$ and Io -- therefore it becomes $Wo < Wo'$ and the PWM of power consumption is smaller compared with constant-current system.

[0014] Next, a wafer short circuit protection network is explained using drawing 4 R> 4. In a normal state, since the signal j from a comparator 67 is not inputted into a latch circuit 68, the latch circuit 68 is always outputting the signal of H to a gate circuit 61 (AND circuit). For this reason, a gate circuit outputs Signal g to the drive circuit 62 according to ON/OFF (H/L) of the PWM signal f. And as shown in drawing 4, the shunt resistance 66 is connected electrically and the electrical potential difference V of the shunt resistance 66 is compared with the wafer 6 by the comparator 67 with the programmed voltage Vset. In a normal state, since it is lower than a programmed voltage Vset, Signal j is not outputted for the electrical potential difference V during shunt resistance from a comparator 67. However, if a wafer 6 short-circuits, since the current beyond a convention will flow to the shunt resistance 66, if the electrical potential difference V of the shunt resistance 66 rises and it becomes large from a programmed voltage Vset, Signal j will be outputted to a latch circuit 68 from a comparator 67. The latch circuit 68 has the function to hold the condition, once Signal j is inputted. For this reason, once Signal j is inputted, the signal of L will always be outputted to a gate circuit 61 (AND circuit). For this reason, the signal g based on the PWM signal f is no

longer outputted to the drive circuit 62, and a circuit is protected from a gate circuit 61. And if a reset switch 69 is pushed after exchanging the wafer which caused short circuit accident, a latch circuit 68 will output the signal of H to a gate circuit 61 (AND circuit). Once reset-signal k is inputted, a latch circuit 68 will hold the condition and will return to a normal state.

[0015] Next, the device of the sterile whole junction equipment 1 is explained. This sterile junction equipment 1 has the 1st clamp 3 and the 2nd clamp 2 which hold at least two flexible tubes in the parallel condition, as shown in drawing 1, drawing 2, drawing 5, and drawing 10. By rotation of the gear 30 rotated by actuation of a motor, the gear 31 rotated by rotation of a gear 30, and a gear 31. The arm 18 for a drive for moving the prevention member 11 for preventing shakiness by the home position of the frame 9 to which the both ends of the shaft 32 to rotate and a shaft were fixed pivotable, and the 1st clamp 3, microswitches 13, 14, and 15, and the 1st clamp 3, and the 1st clamp 3. Shakiness of the cam 17 for making the cam 19, the cutting means 5, the cutting means 5, and the 2nd clamp for making it move drive, the press member 33 which presses the 2nd clamp 2 to the 1st clamp side, the specification-part material 25 which regulates the retreat location of the 1st clamp 3, and the 1st clamp 3. The induction member 26 for guiding the spring member 27 for preventing, the wafer exchange lever 22, the wafer cartridge 8, the wafer cartridge exchange lever 24, the used wafer housing grasping member 28, and a used wafer to a housing, the used wafer housing 29, and a control panel 50. It has.

[0016] And the 1st clamp migration device to which the 1st clamp 3 is moved so that both edges 48a from which this sterile junction equipment 1 was cut by the cutting means 5, and to which the flexible tubes 48 and 49 are joined, and 49a may face each other. It has the locomotive function for making a tubeside move the cutting means 5 (to upper part), and making it move in the direction (caudad) again separated from a tube after cutting, and the 2nd clamp migration device moved in the direction which approaches and estranges the 2nd clamp 2 to the 1st clamp 3. It is what makes it move to a cutting means drive up perpendicularly to the shaft of two tubes, and moves the cutting means 5 to it caudad after tube cutting. The 1st clamp migration device It is what moves the 1st clamp 3 in the rectangular direction in the level condition to the shaft of two tubes (concrete -- back) after tube cutting. the 2nd clamp migration device The 2nd clamp 2 is moved in parallel very only in the level condition to the shaft of two tubes so that the 1st clamp side may be approached.

[0017] Then, the 1st and 2nd clamps 3 and 2 are explained. The 1st and 2nd clamps 3 and 2 are constituted as shown in drawing 1 $R > 1$, drawing 5, drawing 7, and drawing 10. Specifically, the 1st clamp 3 has base 3b, covering 3a attached in this base 3b pivotable, and clamp standing-ways 3c to which base 3b was fixed, as shown in drawing 10. And this clamp standing-ways 3c is being fixed to the linear table. The linear table is constituted by 3n of rail members prepared in the lower part of movable carriage 3c fixed to the inferior surface of tongue of clamp standing-ways 3c, and movable carriage 3c. And on this linear table, to the shaft of the tubes 48 and 49 to join, there is no distortion and the 1st clamp 3 is moved so that a perpendicular direction and both the edges to which in other words the cut flexible tube is joined may face each other. Therefore, the 1st clamp migration device is constituted from sterile junction equipment 1 of this example by the above-mentioned linear table, a motor, a gear 30, the gear 31, the shaft 32, the arm 18 for a drive, and the cam 19. And with this junction equipment 1, as shown in drawing 1 and drawing 5, the spring member 27 which connects the back of 1st clamp standing-ways 3c and the frame of junction equipment 1 is formed, the 1st clamp 3 is in the condition of always having been pulled back, and shakiness of the 1st clamp 3 (correctly 1st clamp standing-ways 3c) is made into few things. Moreover, as shown in drawing 1 $R > 1$ and drawing 5, the prevention member 11 for preventing shakiness of the 1st clamp 2 in the tube stowed position (location in the condition that in other words the 1st clamp came out to the foremost) of the 1st clamp 3 is being fixed to the side face of a frame 9. Therefore, the 1st clamp 3 is in the condition back pulled by the spring member 27, i.e., the condition which does not have shakiness in a back side, and shakes and can move [at a tube stowed position] no longer ahead from it by the prevention member in the front. Therefore, the 1st clamp 3 consists of tube stowed positions so that there may be no shakiness. Moreover, as shown in junction equipment 1 at drawing 1 and drawing 5, the specification-part material 25 which regulates the maximum migration location behind the 1st clamp 3 (correctly 1st clamp standing-ways 3c) is formed.

[0018] The 2nd clamp 2 has clamp standing-ways 2c by which covering 2a attached pivotable and base 2b were fixed to base 2b and this base 2b, as shown in drawing 5, drawing 7, and drawing 10 $R > 0$. And this clamp standing-ways 2c is being fixed to the linear table. The linear table is constituted by 2n of rail members prepared in the lower part of movable carriage 2c fixed to the inferior surface of tongue of clamp standing-ways 2c, and movable carriage 2c. And on this linear table, to the shaft of the tubes 48 and 49 to

join, the 2nd clamp 2 does not have distortion only in an parallel direction and the direction which approaches and estranges the 2nd clamp 2 to the 1st clamp 3, and, in other words, is moved to it.

[0019] Moreover, as shown in drawing 5 and drawing 7, the press member 33 is formed between the frame of junction equipment 1, and clamp standing-ways 2c, and the 2nd clamp 2 (correctly 2nd clamp standing-ways 2c) is always pushed on the 1st clamp side. As a press member, a spring member is used suitably. And when that of a potato is used weakly and the thrust of the press member 33 grasps a flexible tube from the repulsive force of a flexible tube when grasping the 1st and 2nd clamps 3 and 2 as two flexible tubes 48 and 49 were crushed, this press member 33 is constituted so that the 2nd clamp 2 may move in the direction estranged a little from the 1st clamp 3. Therefore, the 2nd clamp migration device is constituted from sterile junction equipment 1 of this example by the above-mentioned linear table, a motor, a gear 30, the gear 31, the shaft 32, the cam 17, and the press member 33.

[0020] And as shown in drawing 10, the 1st clamp 3 and the 2nd clamp 2 are constituted so that the tube to hold may be held in the condition of having crushed aslant. Clamps 3 and 2 have the coverings 3a and 2a attached in base 3b and 2b possible [revolution], and in base 3b and 2b, in order to **** two tubes, they have two slots 3f and 3e established in parallel, and 2f and 2e. And the serrated knife-like lock out members 3h and 2h are formed in the end face of base 3b of the part which Slots 3f and 3e and Slots 2f and 2e face, and 2b. And the lock out members 3g and 2g of the shape of a serrated knife of the configuration corresponding to the lock out members 3h and 2h of the above-mentioned base 3b and 2b are formed in Coverings 3a and 2a. The internal surface of Coverings 3a and 2a is flat. And to Coverings 3a and 2a, it has the revolution cam, respectively, and this revolution cam will engage with the roller of base 3b and 2b, if Coverings 3a and 2a are closed. And when Coverings 3a and 2a are closed, two tubes are aslant crushed by between 3h of lock out members of base 3b, and 3g of lock out members of covering 3a, and between 2h of lock out members of base 2b, and 2g of lock out members of covering 2a, and are held in the condition of having blockaded. Moreover, since the 1st clamp 3 has lobe 3i which projects in the 2nd clamp direction and it has crevice 2i to which the 2nd clamp 2 contains this lobe 3i, the 2nd clamp 2 is constituted so that it cannot blockade, if the 1st clamp 1 is not blockaded.

[0021] And two cams 19 and 17 are being fixed and sterile junction equipment 1 rotates cams 19 and 17 with rotation of a gear 31, as are shown in drawing 1, and it has the gear 30 rotated by the motor, and the gear 31 rotated by rotation of this gear 30 and is shown in the shaft 32 of a gear 31 at drawing 7. And cam-groove 19a for the 1st clamp drive of a configuration as shown in drawing 8 is prepared in the right lateral of a cam 19. And the arm 18 for the 1st clamp migration which has follower 18a which slides on the inside of cam-groove 19a of a cam 19 in the center section is formed. moreover, the lower limit of an arm 18 is supported by the frame 9 rotatable by supporting-point 18b, and the upper limit of an arm 18 is boiled by supporting-point 18c prepared in clamp standing-ways 3c of the 1st clamp 3, and is supported rotatable. Therefore, along with 3n of rail members of a linear table, as shown in drawing 8, the 1st clamp 3 moves to the rectangular direction back in the level condition to the shaft of two tubes by rotation of a cam 19, as shown in an arrow head according to the configuration of cam-groove 19a.

[0022] The cutting means 5 has wafer attaching part 5a which holds a wafer exchangeable, arm section 5c in which wafer attaching part 5a was prepared caudad, follower 5b prepared in the edge of arm section 5c, and 5d of hinge regions and attachment section 5e to a frame 9, as shown in drawing 6. And it can circle to a frame 9 by 5d of hinge regions. And as shown in drawing 6, the temperature detection means 7 for temperature detection of the electrical connection terminal 9 for wafer heating and a wafer is being fixed to the right lateral of the cutting means 5. As a temperature detection means 7, it is desirable that they are a thermocouple or a resistance bulb. ** which is a sheath form thermocouple or a resistance bulb, especially a sheath form thermocouple are desirable more preferably. What has the metal plate bent as a wafer 6 so that it might face each other, the insulating layer formed in the inside of this metal plate, the resistor formed so that the above-mentioned metal plate might not be contacted in this insulating layer, and the terminal for energization prepared in the both ends of this resistor is used suitably.

[0023] And the cam 17 has cam-groove 17a for a cutting means drive in the left lateral, as shown in drawing 6 and drawing 9. And follower 5b of the cutting means 5 is located in cam-groove 17a of a cam 17, and slides on the inside of cam-groove 17a in accordance with the configuration of a cam groove. Therefore, by rotation of a cam 17, as shown in drawing 9, the cutting means 5 will move to a rectangular cross and the perpendicular direction upper and lower sides to the shaft of two tubes, if it puts in another way up and down according to the configuration of cam-groove 17a. Furthermore, the cam 17 has cam-groove 17c for the drive of the 2nd clamp 2 in the center section, as shown in drawing 7. Cam-groove 17c has 17f of left laterals, and right lateral 17e, and controls the location of the 2nd clamp by 17f of left laterals, and right

lateral 17e. In 2nd clamp standing-ways 2c, it has the lobe extended caudad, and the follower 20 is formed at the tip. This follower 20 slides on the inside of cam-groove 17c for the drive of the 2nd clamp 2. And between the side faces of a follower 20 and cam-groove 17c, as shown in drawing 7, it is formed so that the clearance between some may be made. And since 2nd clamp standing-ways 2c is always pushed by the spring member 33, in a normal state, a follower 20 comes to contact 17f of left laterals of cam-groove 17c, and the clearance between some is made between a follower 20 and right lateral 17e of cam-groove 17c. However, as mentioned above, if two tubes are held by the 1st and 2nd clamps 3 and 2, since it blockades and two clamps 3 and 2 hold, respectively so that two tubes may be crushed, they will arise [the repulsive force resulting from lock out of a tube]. And in the condition that clamps 3 and 2 hold a tube, since the thing of the force smaller than the repulsive force resulting from lock out of the above-mentioned tube is used, as shown in drawing 7, a follower 20 comes to contact right lateral 17e of cam-groove 17c, and the clearance between some is made by the spring member 33 between a follower 20 and 17f of left laterals of cam-groove 17c. However, since the repulsive force to which a tube originates in cutting **** and lock out of a tube with the above-mentioned cutting means 5 disappears, return and a follower 20 come to contact 17f of left laterals of cam-groove 17c, and the clearance between some is made in a normal state between a follower 20 and right lateral 17e of cam-groove 17c. Thus, it is constituted so that the sliding surface of the cam groove which a follower 20 contacts may change with an operation of the spring member 33 and the repulsive force of a tube with time.

[0024] And as shown in drawing 7, 17d of crevices is formed in 17f of left laterals. Since the stage when a follower 20 passes 17d part of this crevice is after cutting of a tube by the cutting means, a follower 20 is in the condition which meets and is sliding on 17f of left laterals of a cam groove 17, and, therefore, a follower 20 goes into crevice 17 part. For this reason, the 2nd clamp 2 will move in the 1st clamp 3 direction by the depth of 17d of crevices. Thereby, junction of a tube becomes more certain. And 17g of crevices is established also in right lateral 17e of cam-groove 17c. 17g of this crevice is a thing for cleaning of the inside of clamps 3 and 2. The 2nd clamp 2 can be moved in the direction estranged from the 1st clamp 3, and, thereby, a clearance is formed between the 1st clamp 3 and the 2nd clamp until a follower 20 contacts 17g of crevices by pushing the 2nd clamp 2 on the spring member 33 side by preparing 17g of this crevice. It becomes possible to clean with the cotton swab containing the solvent which can dissolve the formation ingredient of tubes cut to some extent, such as a cleaning member, for example, alcohol etc., into the formed gap. 17g of this crevice is established in the location which faces mostly 17d (part into which ***** of the 2nd clamp 2 is performed) of crevices of 17f of left laterals, as shown in drawing 7. When the follower 20 formed in the lobe to which 2nd clamp standing-ways 2c is extended caudad is contained in 17d part of crevices, it is in the condition which joined both the tubes made into the purpose after tube cutting, and the 2nd clamp stops in this condition. Moreover, the 1st clamp is also already stopped and the 1st clamp 3 is in the location which shifted from the 2nd clamp. As shown in drawing 1, the 1st clamp 3 is retreating from the 2nd clamp 2, and, specifically, the 1st clamp 3 has it in the location which shifted from the 2nd clamp. For this reason, in this condition, the inside of the point of the 2nd clamp 2 is exposed a little, and has also exposed the inside of the back end section of the 1st clamp a little further. Therefore, the cleaning is easy for the inside of the 2nd clamp 2 and the 1st clamp 3 which were exposed.

[0025] Next, an operation of the sterile junction equipment 1 of this invention is explained using a drawing. Drawing 11 is a timing chart which shows actuation of a cutting means, the 1st clamp, and the 2nd clamp. Drawing 12, drawing 13, and drawing 14 are the flow charts for explaining an operation of sterile junction equipment. Drawing 15 R> 5, drawing 16, drawing 17, and drawing 18 are the explanatory views for explaining an operation of sterile junction equipment. With this junction equipment 1, the 1st clamp 3 at the time of junction activity termination serves as a location which shifted from the 2nd clamp 2, and is in the halt location of the timing chart of drawing 11. The include angle of the axis of abscissa of the timing chart of drawing 11 makes 0 degree a zero (condition whose location of the 1st clamp and the 2nd clamp suits), and, in other words, are angle of rotation of the shaft 32 of the subsequent gear 31, and a thing which shows the movement toward the cutting means at the time of angle of rotation of a cam 17 and a cam 19 (wafer), the 1st clamp 3, and the 2nd clamp 2.

[0026] First, as first shown in drawing 12 of a flow chart, the electric power switch 51 prepared in the panel 50 of drawing 3 is pushed. By CPU which constitutes by this the controller 40 shown in drawing 3, when it judges whether it is normal (isn't there any omission of an internal connector, or isn't there specifically any open circuit of a thermocouple, or isn't there any defect in the source of an internal constant voltage?) and there is the above, a buzzer carries out singing of the junction equipment 1. Then, the clamp reset switch 53 prepared in the panel 50 of drawing 3 R> 3 is pushed. By CPU, it judges whether the 1st and 2nd clamps are

open, whether there are any 1st and 2nd clamps in a zero, and whether a wafer exchange lever is in a zero. In addition, since the clamp used with the sterile junction equipment 1 of this example has lobe 3i to which the 1st clamp 3 projects in the 2nd clamp direction as mentioned above and it has crevice 2i to which the 2nd clamp 2 contains this lobe 3i, the 2nd clamp 2 is constituted so that it cannot blockade, if the 1st clamp 1 is not blockaded. For this reason, it is detected by the microswitch 13 with which ON/OFF of the 1st and 2nd clamps being open is carried out by the lever 16 which contacts, and this lever 16 when the 2nd clamp is blockaded. When OFF, a **** cage, and the 2nd clamp 2 are blockaded, a lever 16 is contacted, a lever 16 moves, and, specifically, a microswitch 13 makes a microswitch 13 ON condition, when the 2nd clamp is in a release condition. The ON/OFF signal of this microswitch 13 is inputted into a controller 40. It is judged that there are no 1st and 2nd clamps in a zero when a microswitch SW5 (73) and SW6 (74) detect the slot prepared on the periphery of each cam. It is detected by the microswitch 14 that the wafer exchange lever 22 is in a zero. When a microswitch 14 serves as ON when a lever 22 is in a zero, and there is nothing at a zero, OFF comes and the ON/OFF signal of this microswitch 14 is inputted into a controller 40.

[0027] And as shown in drawing 12, when all four above-mentioned points are YES(s), a motor is operated and the 1st and 2nd clamps are returned to a zero. Moreover, an abnormality lamp puts out the light by in No, BUSA's carrying out singing, and an abnormality lamp's lighting up, performing manual discharge, and pushing at least one reset switch among four above-mentioned points. After the 1st and 2nd clamps arrive at a zero, the 1st and 2nd clamps are equipped with two flexible tubes 48 and 49. The 1st and 2nd clamps 3 and 2 in this condition are in the condition that 2f faced mutually slot 3e which is in the condition which both opened wide, and was prepared for both, and 2e and 3f, as [show / in drawing 10]. And the slots 3f and 2f of a near side are equipped with the tube 49 in use, and the slots 3e and 2e by the side of the back are equipped with the intact tube 48 connected. And after blockading the 1st and 2nd clamps 3 as mentioned above, the wafer exchange lever 22 is pushed on a clamp side, and wafers are exchanged. By pushing the wafer exchange lever 22 on a clamp side, a wafer newer than the inside of the wafer cartridge 8 is taken out, and while push and a standby wafer are equipped with the used wafer with which push and a standby wafer were equipped with the standby wafer with which the cutting means 5 is equipped with a new wafer by the cutting means 5 in an operating location, a used wafer is contained in the used wafer housing 29. By then, CPU which constitutes the controller 40 which will shift to ** of the flow chart of drawing 13 if the initiation switch 52 of a panel 50 is pushed, and is shown in drawing 3 [whether the 1st and 2nd clamps have closed, whether a wafer is exchange settled, and] Whether the 1st and 2nd clamps are in a zero, whether a wafer exchange lever is in a zero, and whether the 1st and 2nd clamps have closed When the 2nd clamp is blockaded, it is detected by the lever 16 which contacts, and the microswitch 13 in which ON/OFF is carried out by this lever 16. When the 2nd clamp is in a release condition, OFF has come, when the 2nd clamp 2 is blockaded, a lever 16 is contacted, a lever 16 moves, and, specifically, a microswitch 13 makes a microswitch 13 ON condition. The ON/OFF signal of this microswitch 13 is inputted into a controller 40. If whether a wafer is exchange settled does push and a wafer exchange activity in the clamp direction for the wafer exchange lever 22, since the exchange lever 22 makes a microswitch 15 turn on once, it will be detected whether it was exchanged by ON signal from a microswitch 15. The ON/OFF signal of a microswitch 15 is inputted into a controller 40. Whether the 1st and 2nd clamps are in a zero detects with microswitches 5 and 6 as mentioned above.

[0028] And as shown in drawing 13, in No, BUSA carries out singing and returns to ** of drawing 12 at least one of the four above-mentioned points. Moreover, when all the four above-mentioned points are YES (s), the working lamp 47 lights up and heating of a wafer is started. it judges whether a wafer current is beyond the set point after heating initiation of a wafer, and a wafer short-circuits this -- **** -- it is for judging. And when a wafer current is not below the set point (the electrical potential difference concerning shunt resistance beyond a predetermined value), after waiting for 0.3 seconds, it judges whether a wafer current is set point within the limits. When a wafer is a used thing, since resistance falls for the heat history of a resistor, this measures a wafer current, detects whether it is in a setting range (inside of tolerance) as compared with the wafer current set up beforehand, and, thereby, judges electrically whether a wafer is used. After BUSA carries out singing, suspending heating of a wafer, and the abnormality lamp in a wafer lighting up and pushing a reset switch when the above-mentioned wafer current is beyond the set point, and when an above-mentioned wafer current is not in a setting range (when the wafer has short-circuited) (when a wafer is used), it shifts to flow chart ** of drawing 12. And heating of a wafer is continued when it is in a setting range (inside of tolerance) as compared with a wafer current. Heating of a wafer 6 is performed controlling the source 43 of a constant voltage by the Pulse-Density-Modulation signal computed based on the temperature detection output of the thermocouple 7 which is a wafer temperature detection means. and

in order to prevent superfluous heating of a wafer, when it judges whether the heating time of a wafer is predetermined within a time, and it judges whether a wafer current is below a predetermined value and the wafer has caused short circuit accident below the predetermined value that is, immediately, BUSA carries out singeing, suspends heating of a wafer, and shifts to flow chart ** of drawing 12. And if the temperature of a wafer reaches laying temperature, it shifts to flow chart ** of drawing 14, and a motor operates, thereby, a gear 30, a gear 31, and cams 19 and 17 will rotate, a cutting means (wafer) will go up, and ***** by the side of cutting of a tube, retreat of the 1st clamp, descent of a cutting means (wafer), and the 1st clamp of the 2nd clamp will be performed.

[0029] If it explains concretely, when a cam 17 rotates in the direction of an arrow head, follower 5b of the cutting means 5 will slide the inside of cam-groove 17a first. From the condition that the zero O of a cam groove shown in drawing 9 and drawing 11 at the beginning touched follower 5b, the point A of cam-groove 17a shown in drawing 9 and drawing 11 comes to contact follower 5b. And as shown in drawing 11, gently-sloping, the cutting means 5 goes up and two flexible tubes are cut from the condition that the point A of cam-groove 17a shown in drawing 9 and drawing 11 contacts follower 5b in the meantime, until the point B of cam-groove 17a results in the condition of contacting follower 5b. If it explains using drawing 15 and drawing 16 $R > 6$, two tubes 48 and 49 are held by the 1st clamp 3 and the 2nd clamp 2, the tube parts 48a and 49a located between the 1st clamp 3 and the 2nd clamp 2 are formed, and the wafer 6 of a cutting means is located in the lower part. And as mentioned above, by rotation of a cam 17, when the cutting means 5 (wafer 6) goes up, as shown in drawing 16, melting cutting of both is carried out in the tube parts 48a and 49a located between the 1st clamp 3 of two tubes, and the 2nd clamp 2.

[0030] And as shown in drawing 9 and drawing 11, the condition that the cutting means 5 went up is maintained, and the edge from which Tubes 48a and 49a were cut is fully dissolved, until it results in the condition that the point C of cam-groove 17a contacts follower 5b from the condition that the point B of cam-groove 17a shown in drawing 9 contacts follower 5b. And as shown in drawing 9 and drawing 11, the cutting means 5 descends gently-sloping, until the point E of cam-groove 17a results [from the condition that the point C of cam-groove 17a shown in drawing 9 and drawing 11 contacts follower 5b] in the condition of contacting follower 5b. Moreover, as shown in drawing 8, when a cam 19 rotates in the direction of an arrow head, follower 18a prepared in the arm 18 for moving the 1st clamp slides the inside of cam-groove 19a. From the condition that the zero O of a cam groove shown in drawing 8 and drawing 11 at the beginning touched follower 18a, the point F of cam-groove 19a shown in drawing 8 and drawing 11 comes to contact follower 18a. As shown in the timing chart of drawing 11, follower 18a results in cam-groove 19 a point F early a little rather than follower 5b of the cutting means 5 results in the point B of cam-groove 17a. And as shown in drawing 11 $R > 1$, gradually, the 1st clamp 3 retreats, will be in the condition which shows in drawing 17 $R > 7$, and will be in the condition that the tube parts 49a and 48a joined faced each other through the wafer 6, until the point G of cam-groove 19a results [from the condition that the point F of cam-groove 19a contacts follower 18a] in the condition contact follower 18a, as shown in drawing 8 $R > 8$ and drawing 11. As shown in the timing chart of drawing 11, this condition is maintained from the condition that the point G of cam-groove 19a contacts follower 18a until the point C of cam-groove 17a results in the condition of contacting follower 5b. And the condition of drawing 17 is maintained until the location of the 1st clamp results [from the condition that Point G contacts follower 18a] in the condition that the point H of cam-groove 19a contacts follower 18a. In addition, as the cutting means 5 is shown in drawing 9 and drawing 11 until the point E of cam-groove 17a results [from the condition that the point C of cam-groove 17a shown in drawing 9 and drawing 11 contacts follower 5b as mentioned above] in the condition of contacting follower 5b, it descends gently-sloping and the tube parts 48a and 49a joined contact.

[0031] And with the time of resulting in the condition which descent of the cutting means 5 ended, and the condition that the point E of cam-groove 17a contacts follower 5b, mostly, as shown in drawing 7 and drawing 11, in other words, the 2nd clamp 2 performs ***** to coincidence at the 1st clamp side. As shown in drawing 7 and drawing 11, specifically the point M of 17d of left laterals of cam-groove 17c Gradually until the point L of a left lateral results [from the condition of contacting the follower 20 for making the 2nd clamp 2 driving] in the condition of contacting a follower 20 the 2nd clamp 2 It moves to the 1st clamp 3 side, and the condition of having ***** (ed) is maintained until the point K of 17d of crevices results [from the condition that the point LK of 17d of crevices of cam-groove 17c contacts a follower 20] in the condition of contacting a follower 20. By this *****, since both of the tube parts 48a and 49a stick certainly, they can make both junction a more positive thing. And gradually, the 2nd clamp 2 moves in the direction separated from the 1st clamp 3 side, and actuation of a motor stops it to this *****

until the point J of 17f of left laterals results [from the condition that the point K of 17d of crevices of cam-groove 17c contacts a follower 20] in the condition of contacting a follower 20.

[0032] Therefore, the 1st clamp 3 in the stopped location serves as location shifted like drawing 17, as the location of the 2nd clamp 2 is shown in drawing 18. And if wafer temperature is detected by the thermocouple and wafer temperature becomes below the set point as shown in the flow chart of drawing 14 $R > 4$, a run light will put out the light and BUSA will carry out singing. And as shown in drawing 18, the junction activity of a tube is completed by opening the 1st clamp 2 and the 2nd clamp 3, and taking out a tube. Moreover, if it puts in another way until the point C of cam-groove 17a results in the condition of contacting follower 5b, from the condition that the point A of cam-groove 17a shown in drawing 7 and drawing 11 contacts follower 5b, although not indicated to the flow chart of drawing 14 It judges whether as shown in the flow chart of drawing 13, a wafer is laying temperature after the cutting means 5 starts a rise also until it starts descent. It is desirable to control the source 43 of a constant voltage by the Pulse-Density-Modulation signal computed based on the temperature detection output of the thermocouple 7 which is a wafer temperature detection means, and to perform temperature control of a wafer. Since the heat of a wafer is absorbed with a tube and this falls when a wafer contacts the tubes 48 and 49 to cut even if a wafer reaches laying temperature once, it is for the compensation ****. The amendment temperature signal b which amended the temperature detection signal a from the thermocouple whose heating control circuit 55 in drawing 4 is the temperature detection means 7 with the PID amendment vessel 56 (proportionality and differential / integral amendment machine 1) which is the amendment wafer temperature calculation section 56, and was amended especially as mentioned above shall be outputted, and it is the amendment Formula 1b=1/K-a-(1+K1 and T-da/dt) ... (1)

If it shall be alike and correction value shall be computed more, since the amendment temperature signal b will have amended the time lag until the actual temperature of the thermocouple which is a temperature detection signal falls by the fall of the temperature of a wafer in K1 and T-da/dt and the fall temperature of an actual wafer is detected correctly, temperature control of a wafer can be performed early [correspondence].

[0033]

[Effect of the Invention] The flexible tube sterile junction equipment of this invention is equipment for joining a flexible tube in sterile. This equipment The 1st clamp and the 2nd clamp which hold at least two flexible tubes in the parallel condition, The cutting means for cutting said flexible tube between this 1st clamp and the 2nd clamp, It has the migration means to which either [at least] said 1st clamp or said 2nd clamp is moved so that both the edges to which the flexible tube cut by this cutting means is joined may stick. A wafer for said cutting means to carry out melting cutting of said flexible tube, It has the source of a constant voltage, wafer temperature detection means, and wafer heating control means for heating this wafer. Said wafer heating control means Based on the output of said wafer temperature detection means, it has the Pulse-Density-Modulation signal output part computed, and said source of a constant voltage is controlled by this Pulse-Density-Modulation signal. By using the source of a constant voltage, and a Pulse-Density-Modulation signal circuit especially, power consumption can be made small, further, by controlling the source of a constant voltage by the Pulse-Density-Modulation signal, temperature control of a wafer for heating melting to cut a flexible tube can be performed certainly, and a positive tube can be joined.

[Translation done.]

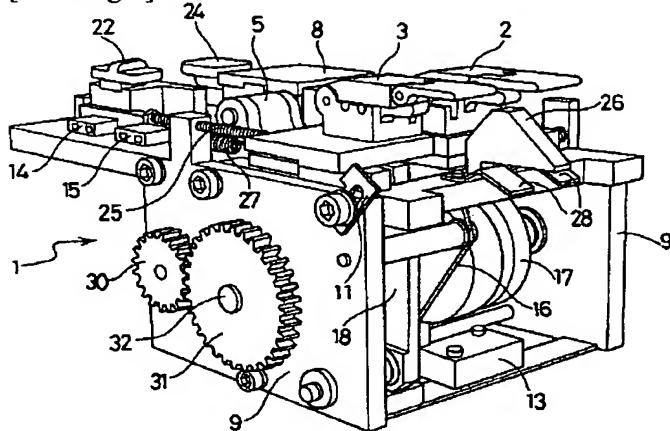
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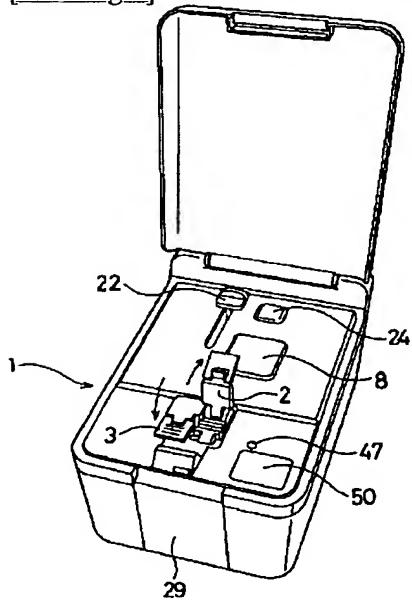
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DRAWINGS

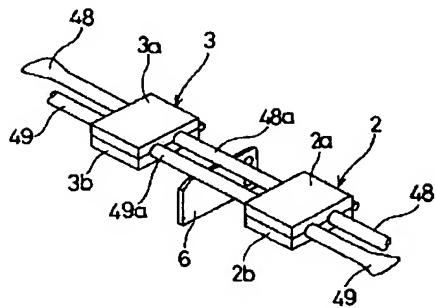
[Drawing 1]



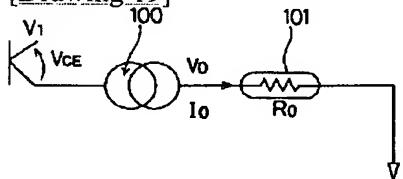
[Drawing 2]



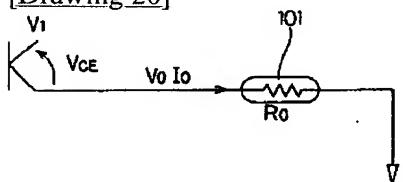
[Drawing 15]



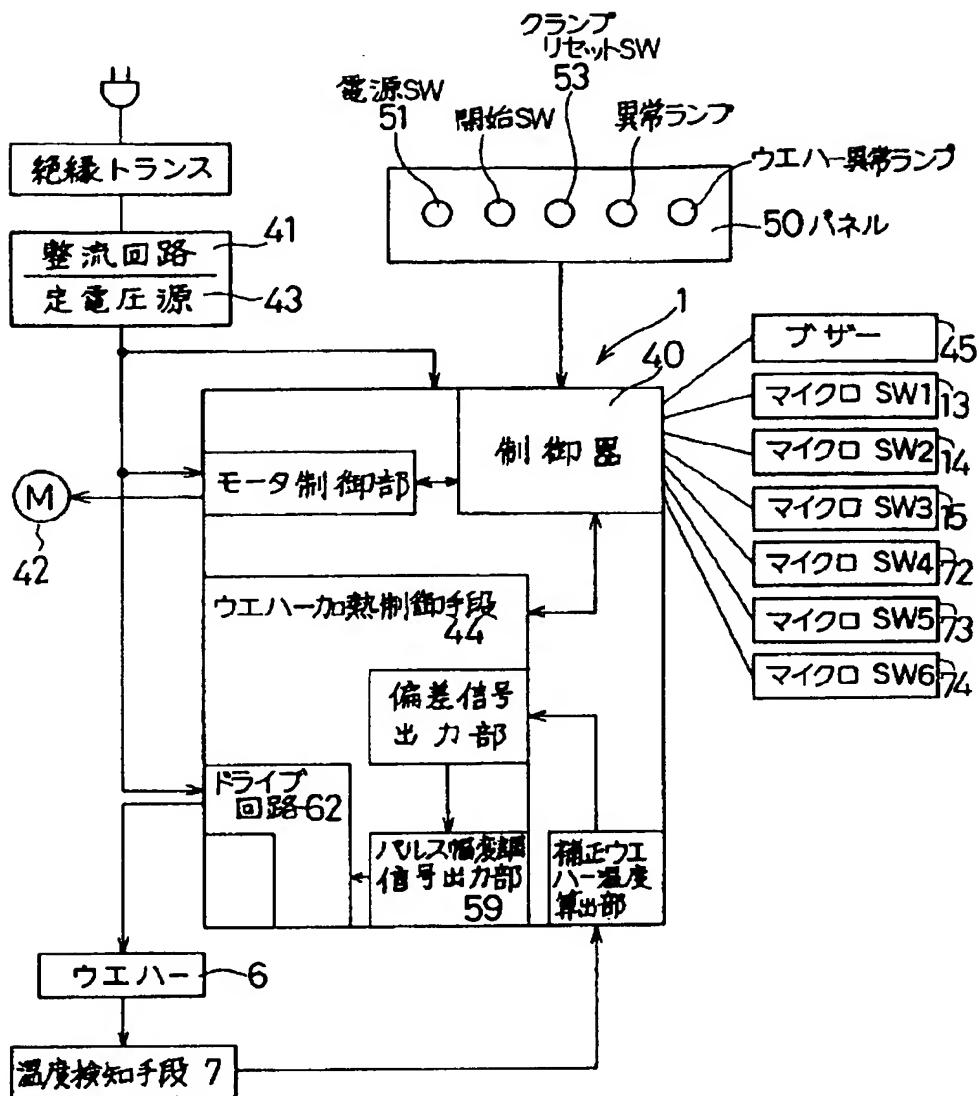
[Drawing 19]



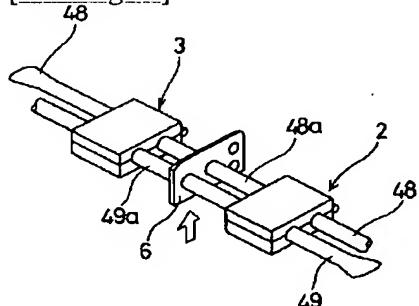
[Drawing 20]



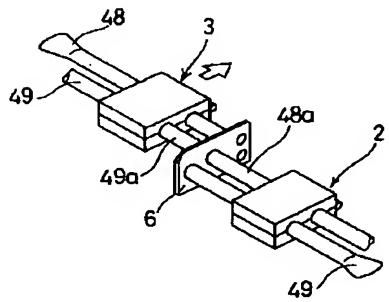
[Drawing 3]



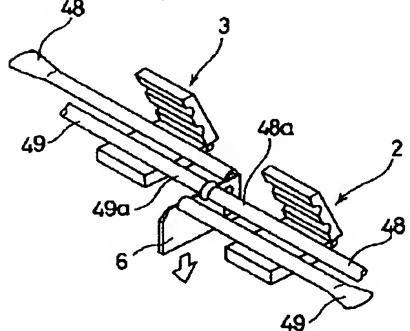
[Drawing 16]



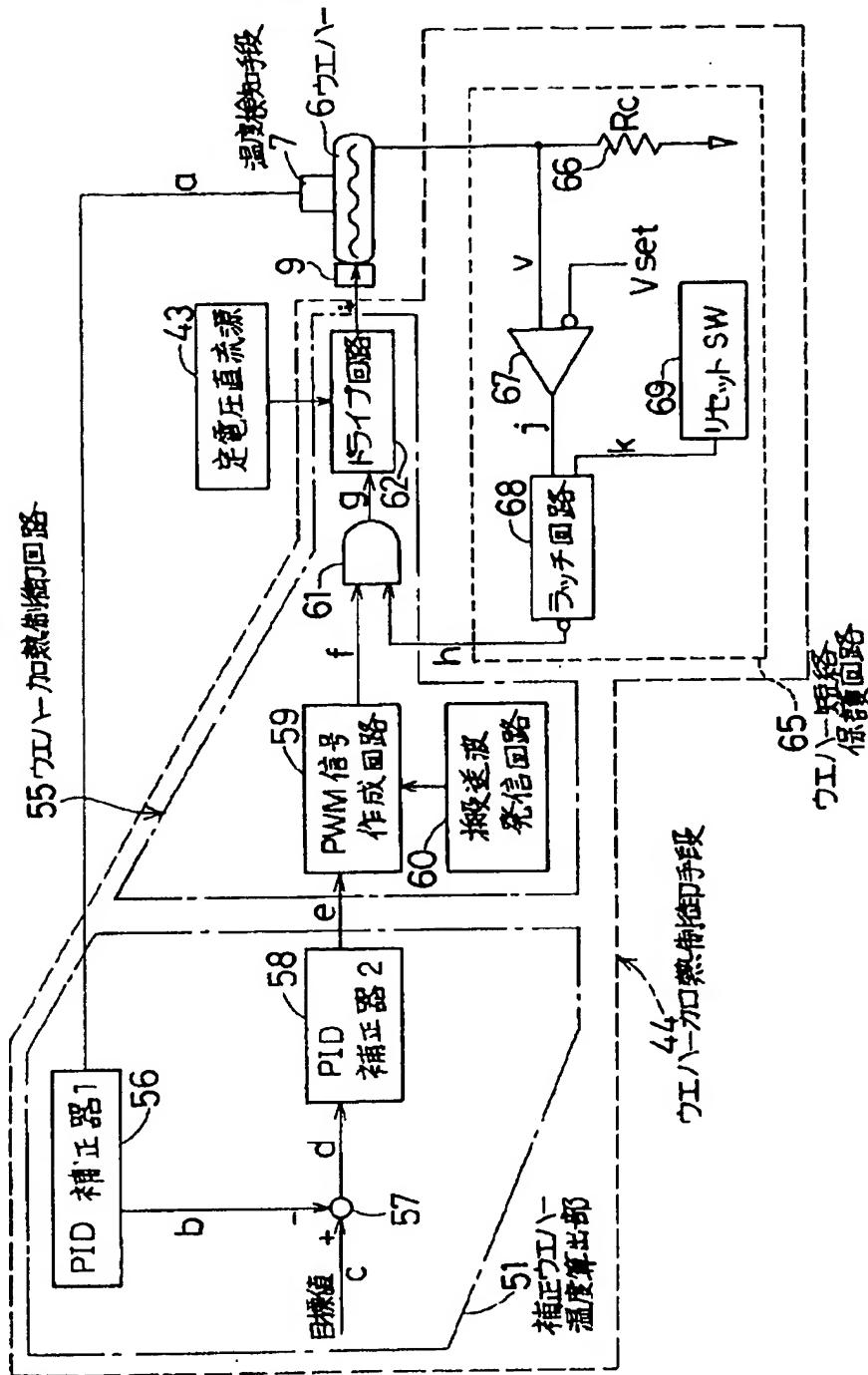
[Drawing 17]



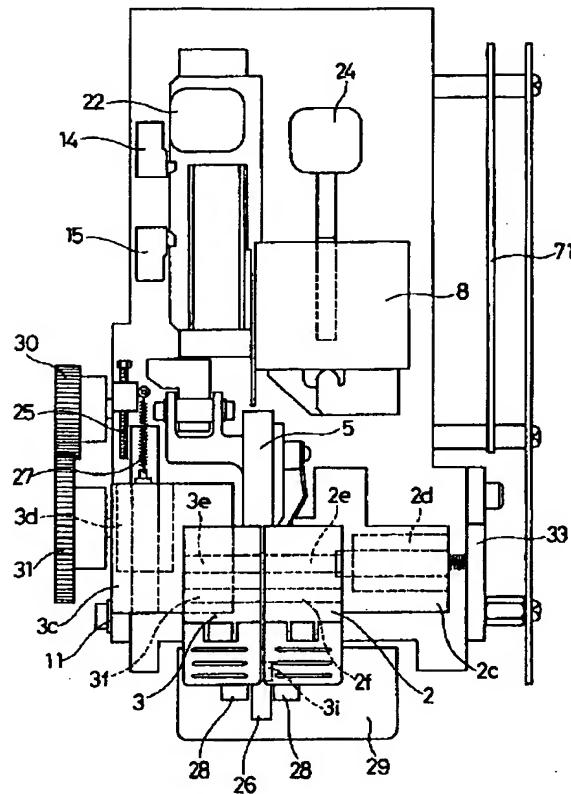
[Drawing 18]



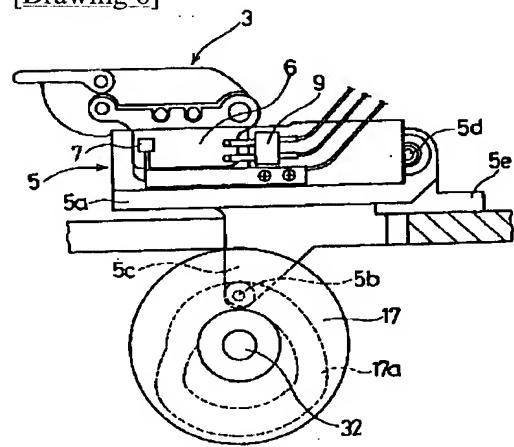
[Drawing 4]



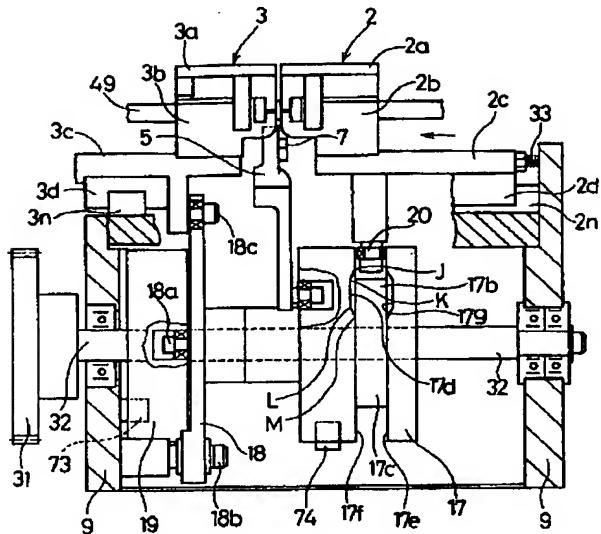
[Drawing 5]



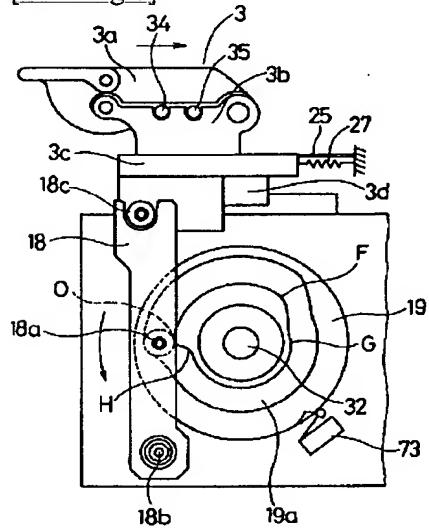
[Drawing 6]



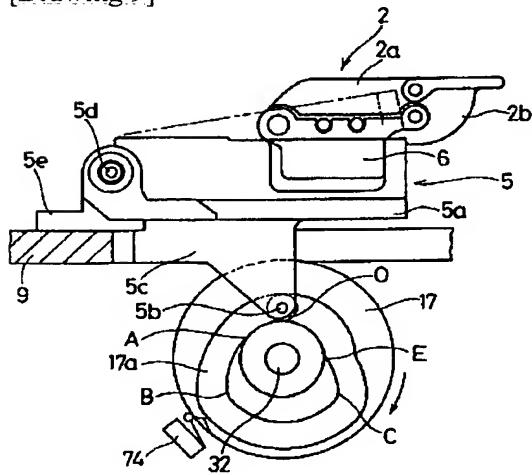
[Drawing 7]



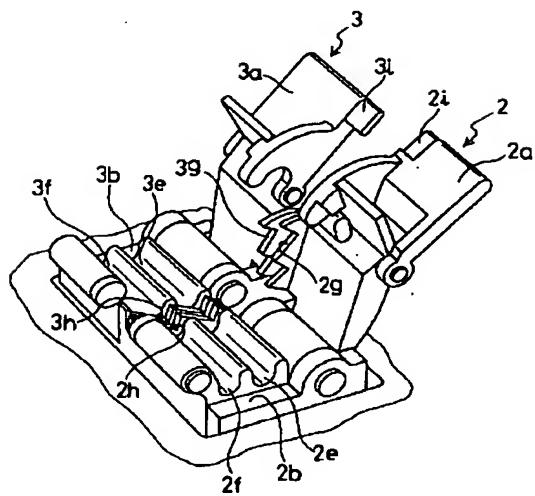
[Drawing 8]



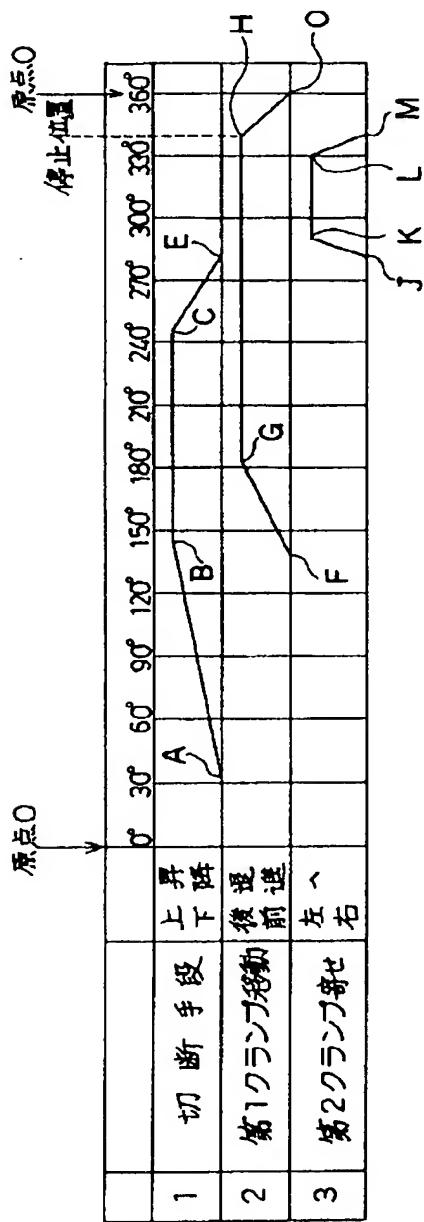
[Drawing 9]



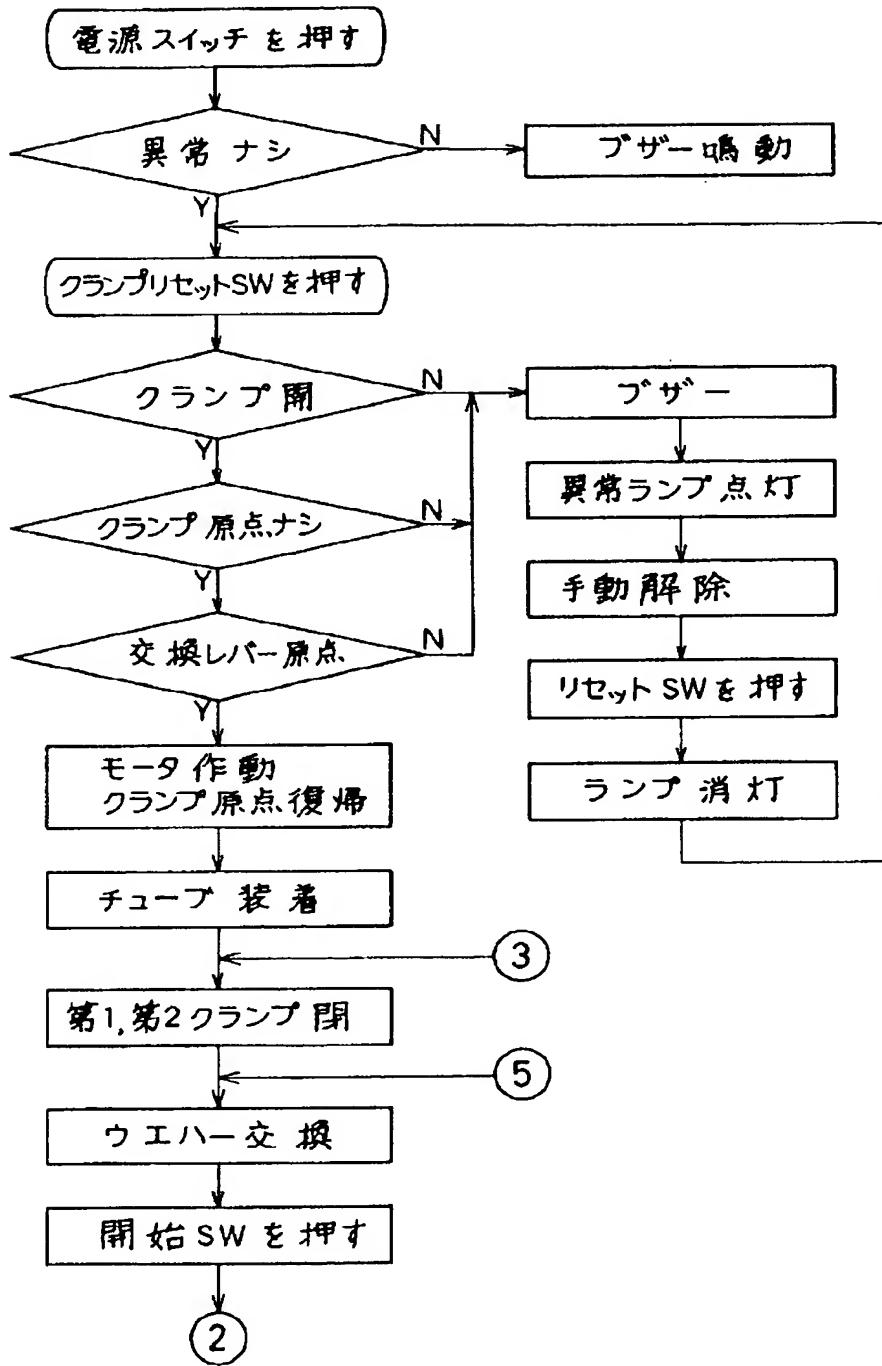
[Drawing 10]



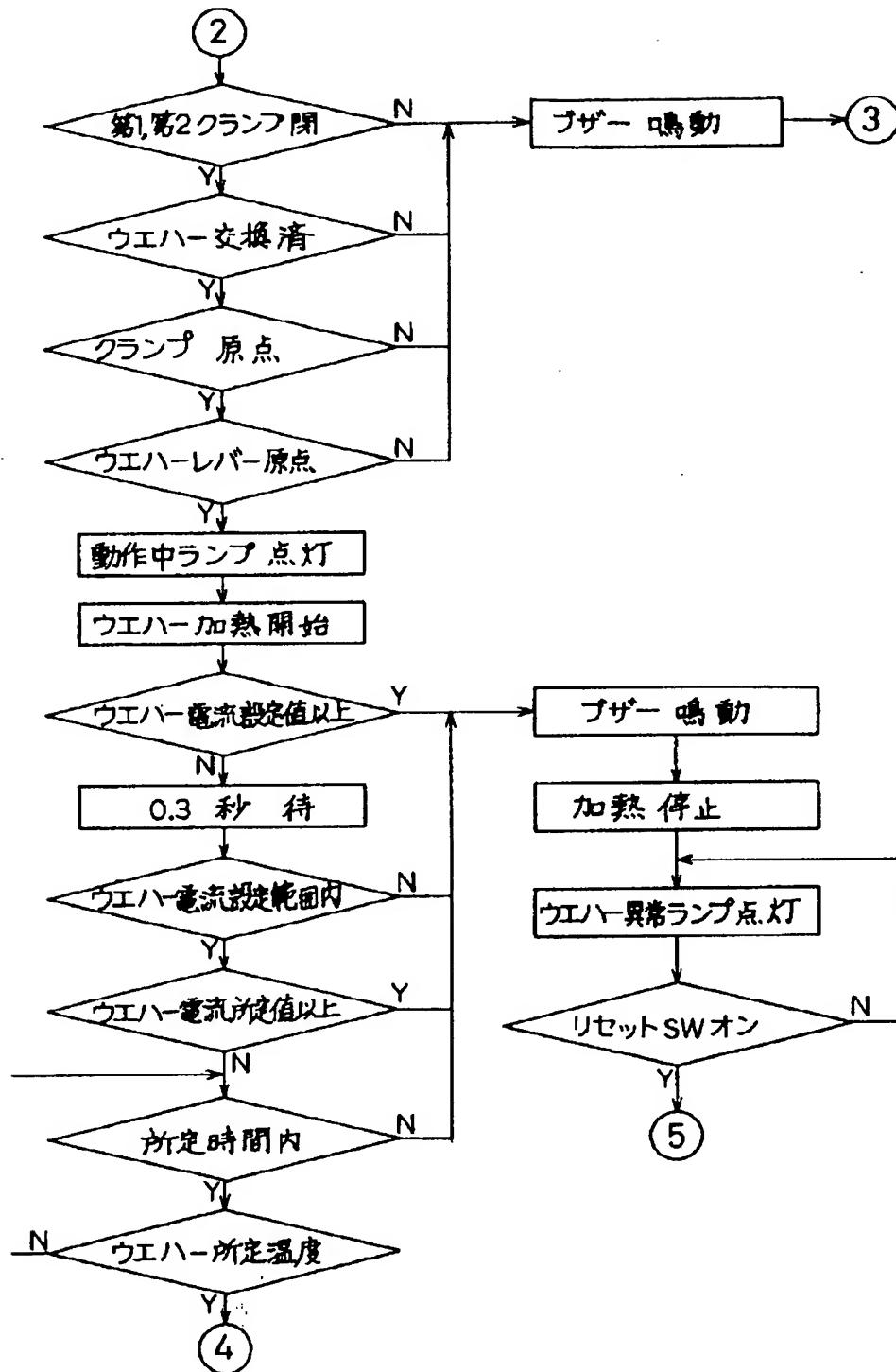
[Drawing 11]



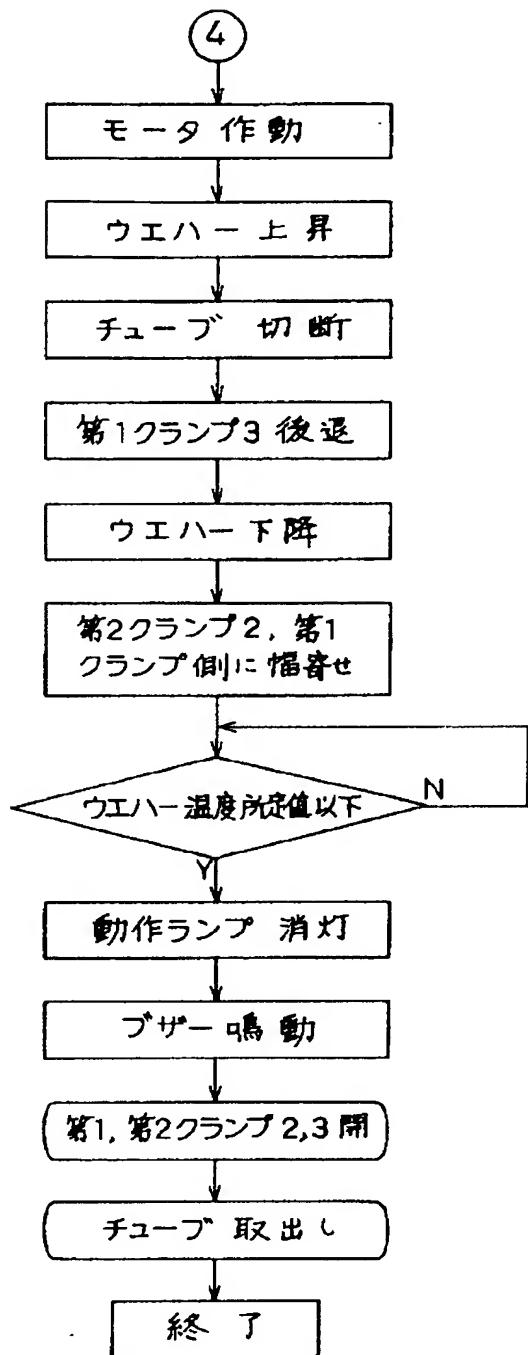
[Drawing 12]



[Drawing 13]



[Drawing 14]



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CORRECTION OR AMENDMENT

[Kind of official gazette] Printing of amendment by the convention of 2 of Article 17 of Patent Law

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A61M 1/28

39/02

[FI]

A61J 1/00 390 M

A61M 1/28

5/14 459 P

[Procedure revision]

[Filing Date] August 31, Heisei 11 (1999. 8.31)

[Procedure amendment 1]

[Document to be Amended] Specification

[Item(s) to be Amended] Whole sentence

[Method of Amendment] Modification

[Proposed Amendment]

[Document Name] Specification

[Title of the Invention] Flexible tube sterile junction equipment

[Claim(s)]

[Claim 1] It is flexible tube sterile junction equipment which is equipped with the following, and said wafer heating control means has the Pulse-Density-Modulation signal output part computed based on the output of said wafer temperature detection means, and is characterized by being what controls said source of a constant voltage by this Pulse-Density-Modulation signal. It is the 1st clamp and the 2nd clamp to which it is equipment for joining a flexible tube in sterile, and this equipment holds a tube. It is a wafer to have a cutting means for cutting said flexible tube between this 1st clamp and the 2nd clamp, and for said cutting means carry out melting cutting of the flexible tube. The source of a constant voltage for heating this wafer A wafer temperature detection means and a wafer heating control means

[Claim 2] Flexible tube sterile junction equipment according to claim 1 characterized by providing the following Said flexible tube sterile junction equipment is the 1st clamp and the 2nd clamp which hold at least two flexible tubes in the parallel condition. The cutting means for cutting said flexible tube between this 1st clamp and the 2nd clamp The migration means to which either [at least] said 1st clamp or said 2nd clamp is moved so that both the edges to which the flexible tube cut by this cutting means is joined may stick

[Claim 3] It is flexible tube sterile junction equipment according to claim 1 or 2 which is that to which said

wafer heating control means has the deflection signal output part which outputs the deflection signal of the amendment wafer temperature calculation section, the amendment temperature computed by this calculation section, and whenever [purpose stoving temperature / of said wafer] based on the output of said wafer temperature detection means, and said Pulse-Density-Modulation signal output part outputs a Pulse-Density-Modulation signal based on this deflection signal.

[Claim 4] Said wafer heating control means is flexible tube sterile junction equipment according to claim 1 to 3 which has the wafer short circuit protection network.

[Claim 5] It is flexible tube sterile junction equipment according to claim 4 with which said wafer short circuit protection network has the short circuit detection section of said wafer, and the pulse-width-modulation signal-control section which controls an inflow in said drive circuit of the pulse-width-modulation signal from said pulse-width-modulation signal output part based on the detection signal of this short circuit detection section by said wafer heating control means having the drive circuit for controlling said source of a constant voltage by this pulse-width-modulation signal.

[Claim 6] Said amendment wafer temperature calculation section is flexible tube sterile junction equipment according to claim 3 which has proportionality, the integral, and the differential correction circuit.

[Claim 7] Said deflection signal output part is flexible tube sterile junction equipment according to claim 3 which has proportionality, the integral, and the differential correction circuit.

[Detailed Description of the Invention]

[0001]

[Industrial Application] This invention carries out heating fusion of at least two flexible tubes, and relates to the flexible tube sterile junction equipment for connecting in sterile.

[0002]

[Description of the Prior Art] At the time of tube connection of the blood collecting bag in a transfusion system and a constituent-of-blood bag, and exchange of the dialysing fluid bag in continuous ambulatory PD (CAPD), and a waste fluid bag, it is necessary to connect a tube in sterile. There are some which are shown in JP,61-30582,B as equipment which makes sterile connection of such a tube. The equipment shown in this JP,61-30582,B is a tube contact which carries out heating fusion of the tube and is connected. It has a cutting means for cutting a flexible tube between the 1st clamp and the 2nd clamp which hold two flexible tubes which should be connected in the parallel condition, and the 1st clamp and the 2nd clamp, and the migration means to which either [at least] the 1st clamp or the 2nd clamp is moved so that both the edges to which the flexible tube cut by the cutting means is joined may stick.

[0003] And the cutting means has the wafer for carrying out melting cutting of the flexible tube, and the power source for heating a wafer. As a power source for heating a wafer, the constant current source is used as shown in JP,59-64034,A. And the approach of predicting the temperature of a wafer from resistance is used for the temperature control of a wafer using the resistance temperature change of a resistor.

[0004]

[Problem(s) to be Solved by the Invention] However, by the approach the temperature control of a wafer predicts the temperature of a wafer from resistance using the resistance temperature change of a resistor using a constant current source, it actually has the trouble that it is difficult to perform positive temperature control since the temperature of a wafer is measured and it does not control as shown in JP,59-64034,A. Furthermore, in the heating circuit using a constant current source, since loss of a drive circuit was large, there was also a trouble that power consumption was large. Then, the purpose of this invention can perform certainly temperature control of a wafer for heating melting to cut a flexible tube, and offers flexible tube sterile junction equipment with little power consumption further.

[0005]

[Means for Solving the Problem] It is equipment for joining a flexible tube in sterile which attains the above-mentioned purpose. This equipment It has a cutting means for cutting said flexible tube between the 1st clamp and the 2nd clamp holding a tube, and this 1st clamp and the 2nd clamp. Said cutting means The source of a constant voltage for heating the wafer and this wafer for carrying out melting cutting of the flexible tube, It has a wafer temperature detection means and a wafer heating control means. Said wafer heating control means It is flexible tube sterile junction equipment which is what has the Pulse-Density-Modulation signal output part computed based on the output of said wafer temperature detection means, and controls said source of a constant voltage by this Pulse-Density-Modulation signal. It is equipment for joining a flexible tube in sterile which attains the above-mentioned purpose. Moreover, this equipment The 1st clamp and the 2nd clamp which hold at least two flexible tubes in the parallel condition, The cutting means for cutting said flexible tube between this 1st clamp and the 2nd clamp, It has the migration means to

which either [at least] said 1st clamp or said 2nd clamp is moved so that both the edges to which the flexible tube cut by this cutting means is joined may stick. A wafer for said cutting means to carry out melting cutting of said flexible tube, It has the source of a constant voltage, wafer temperature detection means, and wafer heating control means for heating this wafer. Said wafer heating control means It is flexible tube sterile junction equipment which is what has the Pulse-Density-Modulation signal output part computed based on the output of said wafer temperature detection means, and controls said source of a constant voltage by this Pulse-Density-Modulation signal.

[0006] And said wafer heating control means has the deflection signal output part which outputs the deflection signal of the amendment wafer temperature calculation section, the amendment temperature computed by this calculation section, and whenever [purpose stoving temperature / of said wafer] based on the output of said wafer temperature detection means, and, as for said Pulse-Density-Modulation signal output part, it is desirable that it is what outputs a Pulse-Density-Modulation signal based on this deflection signal. Furthermore, as for said wafer heating control means, it is desirable to have the wafer short circuit protection network. Moreover, said wafer heating control means has the drive circuit for controlling said source of a constant voltage by this pulse-width-modulation signal, and, as for said wafer short circuit protection network, it is desirable to have the short circuit detection section of said wafer and the pulse-width-modulation signal-control section which controls an inflow in said drive circuit of the pulse-width-modulation signal from said pulse-width-modulation signal output part based on the detection signal of this short circuit detection section. Moreover, as for said amendment wafer temperature calculation section, it is desirable to have proportionality, the integral, and the differential correction circuit. Furthermore, as for said deflection signal output part, it is desirable to have proportionality, the integral, and the differential correction circuit. And as for said wafer temperature detection means, it is desirable that they are a thermocouple or a resistance bulb. Furthermore, as for said wafer temperature detection means, it is desirable that they are a sheath form thermocouple or a resistance bulb.

[0007] Then, the flexible tube sterile junction equipment of this invention is explained with reference to a drawing. The 1st clamp 3 and the 2nd clamp 2 which this flexible tube sterile junction equipment 1 is equipment for joining a flexible tube in sterile, and hold at least two flexible tubes in the parallel condition, The cutting means 5 for cutting the flexible tubes 48 and 49 between the 1st clamp 3 and the 2nd clamp 2, It has the migration means to which either [at least] the 1st clamp 3 or the 2nd clamp 2 is moved so that both edges 48a to which the flexible tubes 48 and 49 cut by the cutting means 5 are joined, and 49a may stick. The wafer 6 for the cutting means 5 to carry out melting cutting of the flexible tubes 48 and 49, It has the source 43 of a constant voltage, the wafer temperature detection means 7, and the wafer heating control means 44 for heating a wafer 6. The wafer heating control means 44 Based on the output of the wafer temperature detection means 7, it has the Pulse-Density-Modulation signal output part 59 computed, and the source 43 of a constant voltage is controlled by the Pulse-Density-Modulation signal.

[0008] Drawing 1 is the perspective view of one example of the flexible tube sterile junction equipment of this invention, drawing 2 is the perspective view showing the condition contained in the case the sterile junction equipment shown in drawing 1, drawing 3 is the block diagram showing an example of the electrical circuit used for the sterile junction equipment of this invention, and drawing 4 is the electrical circuit block diagram showing an example of the wafer heating control means of the electrical circuit of the sterile junction equipment of this invention. Drawing 5 is the plan of one example of the flexible tube sterile junction equipment of this invention.

[0009] Next, the wafer heating control means indicated to drawing 4 is explained. What has the metal plate bent as a wafer 6 so that it might face each other, the insulating layer formed in the inside of this metal plate, the resistor formed so that the above-mentioned metal plate might not be contacted in this insulating layer, and the terminal for energization prepared in the both ends of this resistor is used suitably. And since a resistor generates heat by energization, generation of heat of a resistor is conducted to a metal plate, and the whole wafer generates heat by energization. And resistance changes with generation of heat according [a resistor] to energization. Therefore, the source of a constant voltage is only used and temperature control of enough wafers cannot be performed only by adjusting the electric power supply to a wafer. So, with the sterile junction equipment 1 of this example, it has the wafer heating control means.

[0010] As shown in drawing 4, as for the wafer heating control means 44, it is desirable to have the wafer heating control circuit 55 and the amendment wafer temperature calculation section 51, and to have the wafer short circuit protection network 65 further, as shown in drawing 4. The wafer heating control circuit 55 has the Pulse-Density-Modulation signal output part 59 computed based on the output from the temperature detection means 7, and controls the source 43 of a constant voltage by the Pulse-Density-

Modulation signal. Having the deflection signal output part 57 which outputs the deflection signal of the amendment temperature specifically computed by the amendment wafer temperature calculation section 56 which computes amendment wafer temperature, and the calculation section based on the output of the wafer temperature detection means 7, and whenever [purpose stoving temperature / of a wafer], the Pulse-Density-Modulation signal output part 59 outputs a Pulse-Density-Modulation signal based on a deflection signal. As a temperature detection means 7, it is desirable that they are a thermocouple or a resistance bulb. More preferably, it is a sheath form thermocouple or a resistance bulb, and a sheath form thermocouple is desirable especially.

[0011] If the heating control means 44 is more concretely explained using drawing 4, the temperature detection signal a from the thermocouple which is the temperature detection means 7 will be inputted into the PID amendment machine 56 (proportionality and differential / integral amendment machine 1) of the amendment wafer temperature calculation section 51, and the amended amendment temperature signal b will be outputted. With this PID amendment machine 56, it is a formula 1, for example.

$$b=1/-K-a \cdot (1+K1 \text{ and } T \cdot da/dt) \dots (1)$$

It is alike and correction value is computed more. K is the coupling coefficient of a wafer and a thermocouple, K1 is a correction factor resulting from the flexible tube cut, and T is the thermal time constant of a thermocouple. The purpose which performs such amendment is to perform [performing amendment (K) based on the heat-conduction loss between a wafer and a thermocouple, and] amendment in consideration of the thermal time constant (T) of a thermocouple. And as shown in a formula 1, the amendment temperature signals $1/K$ are highly computed by K1 and $T \cdot da/dt$, while wafer temperature is rising from the surveyed wafer temperature signal a, since b is a constant. The temperature which a thermocouple detects is the internal temperature of a thermocouple, and has delay to the skin temperature of a wafer. However, since the delay of a thermocouple is approximated to first-order lag, it considers as a time constant T and the primary progress operation of a time constant T is conversely performed as a correction function by performing the above-mentioned amendment, wafer skin temperature is correctly [without a time lag] computable.

[0012] Moreover, exact wafer skin temperature is correctly [without a time lag] computable by performing amendment as shown in a formula 1 also at the time of wafer temperature descent. And it will become a formula 2 if a formula 1 is rewritten in consideration of a sampling time (**t).

$$b(t+**t) = 1/-K-a(t+**t) \text{ and } \{1+K1 \cdot T/**t - [a(t+**t) - a(t)]\} \dots (2)$$

Thus, the amendment temperature signal b computed is compared with the target wafer temperature signal c, and the deflection signal d is outputted by the deflection signal output part 57. This deflection signal d is inputted into the PID amendment machine 2 designed by the suitable transfer function in order to raise the responsibility of a control system, and it is outputted as an amendment deflection signal e. This amendment deflection signal e is inputted into the Pulse-Density-Modulation signal output part (PWM signal creation circuit) 59. The PWM signal creation circuit 59 synchronizes with the predetermined frequency created by the above-mentioned amendment deflection signal e and the above-mentioned subcarrier oscillator circuit 60, and outputs the signal (pulse train signal which carried out the PWM modulation) f of the pulse width proportional to the amendment deflection signal e. This pulse train signal f passes along a gate circuit 61, and flows into the drive circuit 62. The drive circuit 62 is constituted by a transistor, a thyristor, etc. which are a solid-state-switching component, inputted pulse train signal g acts as switching and a timing signal, and only when pulse train signal g is in the condition of H, the source of a constant voltage and a wafer are connected. Connection between the drive circuit 62 and a wafer 6 is made with the connection terminal 39. The source 43 of a constant voltage and a wafer 6 are intermittently connected based on pulse train signal g, and a wafer is controlled by the wafer temperature made into the purpose.

[0013] And when the outline of the heating circuit in the case of constant-current system comes to be shown in drawing 19 and loss of the heating circuit of constant-current system is searched for, loss (W_o') is $W_o' = (V_i - V_o) I_o$ and is $W_o' = [V_{ce} + \{(V_i - V_{ce}) - V_o\}] I_o$. It is set to (A). Moreover, the outline of the heating circuit in the case of PWM comes to be shown in drawing 20, and loss (W_o) of a drive circuit is, It is $W_o = V_o / V_i - V_{ce} - I_o + W_1$ (B),

W_1 is the switching loss of the transistor which constitutes a drive circuit. And generally a comparison of W_o and W_o' materializes the following relation in B type.

$$V_o / V_i - V_{ce} - I_o > W_1$$

Next, generally in A type, the following relation is realized.

$$V_{ce} < (V_i - V_{ce}) - V_o$$

If this compares the 1st item of A type and B type, and the 2nd item,
 $Vo/Vi-Vce-Io < Vce-Io$
 $W1 < (Vi-Vce)-Vo$, Io

Therefore, it becomes $Wo < Wo'$ and the PWM of power consumption is smaller compared with constant-current system.

[0014] Next, a wafer short circuit protection network is explained using drawing 4. In a normal state, since the signal j from a comparator 67 is not inputted into a latch circuit 68, the latch circuit 68 is always outputting the signal of H to a gate circuit 61 (AND circuit). For this reason, a gate circuit outputs Signal g to the drive circuit 62 according to ON/OFF (H/L) of the PWM signal f . And as shown in drawing 4, the shunt resistance 66 is connected electrically and the electrical potential difference V of the shunt resistance 66 is compared with the wafer 6 by the comparator 67 with the programmed voltage $Vset$. In a normal state, since it is lower than a programmed voltage $Vset$, Signal j is not outputted for the electrical potential difference V during shunt resistance from a comparator 67. However, if a wafer 6 short-circuits, since the current beyond a convention will flow to the shunt resistance 66, if the electrical potential difference V of the shunt resistance 66 rises and it becomes large from a programmed voltage $Vset$, Signal j will be outputted to a latch circuit 68 from a comparator 67. The latch circuit 68 has the function to hold the condition, once Signal j is inputted. For this reason, once Signal j is inputted, the signal of L will always be outputted to a gate circuit 61 (AND circuit). For this reason, the signal g based on the PWM signal f is no longer outputted to the drive circuit 62, and a circuit is protected from a gate circuit 61. And if a reset switch 69 is pushed after exchanging the wafer which caused short circuit accident, a latch circuit 68 will output the signal of H to a gate circuit 61 (AND circuit). Once reset-signal k is inputted, a latch circuit 68 will hold the condition and will return to a normal state.

[0015] Next, the device of the sterile whole junction equipment 1 is explained. This sterile junction equipment 1 has the 1st clamp 3 and the 2nd clamp 2 which hold at least two flexible tubes in the parallel condition, as shown in drawing 1, drawing 2, drawing 5, and drawing 10. By rotation of the gear 30 rotated by actuation of a motor, the gear 31 rotated by rotation of a gear 30, and a gear 31. The arm 18 for a drive for moving the prevention member 11 for preventing shakiness by the home position of the frame 9 to which the both ends of the shaft 32 to rotate and a shaft were fixed pivotable, and the 1st clamp 3, microswitches 13, 14, and 15, and the 1st clamp 3, and the 1st clamp 3. Shakiness of the cam 17 for making the cam 19, the cutting means 5, the cutting means 5, and the 2nd clamp for making it move drive, the press member 33 which presses the 2nd clamp 2 to the 1st clamp side, the specification-part material 25 which regulates the retreat location of the 1st clamp 3, and the 1st clamp 3. The induction member 26 for guiding the spring member 27 for preventing, the wafer exchange lever 22, the wafer cartridge 8, the wafer cartridge exchange lever 24, the used wafer housing grasping member 28, and a used wafer to a housing, the used wafer housing 29, and a control panel 50. It has.

[0016] And it is characterized by equipping this sterile junction equipment 1 with the following. The 1st clamp migration device to which the 1st clamp 3 is moved so that both edges 48a to which the flexible tubes 48 and 49 cut by the cutting means 5 are joined, and 49a may face each other. The locomotive function for making a tubeside move the cutting means 5 (to upper part), and making it move in the direction (caudad) again separated from a tube after cutting. The 2nd clamp migration device moved in the direction which approaches and estranges the 2nd clamp 2 to the 1st clamp 3. It is what makes it move to a cutting means drive up perpendicularly to the shaft of two tubes, and moves the cutting means 5 to it caudad after tube cutting. The 1st clamp migration device It is what moves the 1st clamp 3 in the rectangular direction in the level condition to the shaft of two tubes (concrete -- back) after tube cutting. the 2nd clamp migration device The 2nd clamp 2 is moved in parallel very only in the level condition to the shaft of two tubes so that the 1st clamp side may be approached.

[0017] Then, the 1st and 2nd clamps 3 and 2 are explained. The 1st and 2nd clamps 3 and 2 are constituted as shown in drawing 1, drawing 5, drawing 7, and drawing 10. Specifically, the 1st clamp 3 has base 3b, covering 3a attached in this base 3b pivotable, and clamp standing-ways 3c to which base 3b was fixed, as shown in drawing 10. And this clamp standing-ways 3c is being fixed to the linear table. The linear table is constituted by 3n of rail members prepared in the lower part of 3d of movable carriages fixed to the inferior surface of tongue of clamp standing-ways 3c, and 3d of movable carriages. And on this linear table, to the shaft of the tubes 48 and 49 to join, there is no distortion and the 1st clamp 3 is moved so that a perpendicular direction and both the edges to which in other words the cut flexible tube is joined may face each other. Therefore, the 1st clamp migration device is constituted from sterile junction equipment 1 of this example by the above-mentioned linear table, a motor, a gear 30, the gear 31, the shaft 32, the arm 18 for a

drive, and the cam 19. And with this junction equipment 1, as shown in drawing 1 and drawing 5, the spring member 27 which connects the back of 1st clamp standing-ways 3c and the frame of junction equipment 1 is formed, the 1st clamp 3 is in the condition of always having been pulled back, and shakiness of the 1st clamp 3 (correctly 1st clamp standing-ways 3c) is made into few things. Moreover, as shown in drawing 1 and drawing 5, the prevention member 11 for preventing shakiness of the 1st clamp 3 in the tube stowed position (location in the condition that in other words the 1st clamp came out to the foremost) of the 1st clamp 3 is being fixed to the side face of a frame 9. Therefore, the 1st clamp 3 is in the condition back pulled by the spring member 27, i.e., the condition which does not have shakiness in a back side, and shakes and can move [at a tube stowed position] no longer ahead from it by the prevention member in the front. Therefore, the 1st clamp 3 consists of tube stowed positions so that there may be no shakiness. Moreover, as shown in junction equipment 1 at drawing 1 and drawing 5, the specification-part material 25 which regulates the maximum migration location behind the 1st clamp 3 (correctly 1st clamp standing-ways 3c) is formed.

[0018] The 2nd clamp 2 has clamp standing-ways 2c by which covering 2a attached pivotable and base 2b were fixed to base 2b and this base 2b, as shown in drawing 5, drawing 7, and drawing 10. And this clamp standing-ways 2c is being fixed to the linear table. The linear table is constituted by 2n of rail members prepared in the lower part of 2d of movable carriages fixed to the inferior surface of tongue of clamp standing-ways 2c, and 2d of movable carriages. And on this linear table, to the shaft of the tubes 48 and 49 to join, the 2nd clamp 2 does not have distortion only in an parallel direction and the direction which approaches and estranges the 2nd clamp 2 to the 1st clamp 3, and, in other words, is moved to it.

[0019] Moreover, as shown in drawing 5 and drawing 7, the press member 33 is formed between the frame of junction equipment 1, and clamp standing-ways 2c, and the 2nd clamp 2 (correctly 2nd clamp standing-ways 2c) is always pushed on the 1st clamp side. As a press member, a spring member is used suitably. And when the weak thing is used and the thrust of the press member 33 grasps a flexible tube from the repulsive force of a flexible tube when grasping as two flexible tubes 48 and 49 were crushed by the 1st and 2nd clamps 3 and 2, this press member 33 is constituted so that the 2nd clamp 2 may move in the direction estranged a little from the 1st clamp 3. Therefore, the 2nd clamp migration device is constituted from sterile junction equipment 1 of this example by the above-mentioned linear table, a motor, a gear 30, the gear 31, the shaft 32, the cam 17, and the press member 33.

[0020] And as shown in drawing 10, the 1st clamp 3 and the 2nd clamp 2 are constituted so that the tube to hold may be held in the condition of having crushed aslant. Clamps 3 and 2 have the coverings 3a and 2a attached in base 3b and 2b possible [revolution], and in base 3b and 2b, in order to lay two tubes, they have two slots 3f and 3e established in parallel, and 2f and 2e. And the serrated knife-like lock out members 3h and 2h are formed in the end face of base 3b of the part which Slots 3f and 3e and Slots 2f and 2e face, and 2b. And the lock out members 3g and 2g of the shape of a serrated knife of the configuration corresponding to the lock out members 3h and 2h of the above-mentioned base 3b and 2b are formed in Coverings 3a and 2a. The internal surface of Coverings 3a and 2a is flat. And to Coverings 3a and 2a, it has the revolution cam, respectively, and this revolution cam will engage with the roller of base 3b and 2b, if Coverings 3a and 2a are closed. And when Coverings 3a and 2a are closed, two tubes are aslant crushed by between 3h of lock out members of base 3b, and 3g of lock out members of covering 3a, and between 2h of lock out members of base 2b, and 2g of lock out members of covering 2a, and are held in the condition of having blockaded. Moreover, since the 1st clamp 3 has lobe 3i which projects in the 2nd clamp direction and it has crevice 2i to which the 2nd clamp 2 contains this lobe 3i, the 2nd clamp 2 is constituted so that it cannot blockade, if the 1st clamp 3 is not blockaded.

[0021] And two cams 19 and 17 are being fixed and sterile junction equipment 1 rotates cams 19 and 17 with rotation of a gear 31, as are shown in drawing 1, and it has the gear 30 rotated by the motor, and the gear 31 rotated by rotation of this gear 30 and is shown in the shaft 32 of a gear 31 at drawing 7. And cam-groove 19a for the 1st clamp drive of a configuration as shown in drawing 8 is prepared in the right lateral of a cam 19. And the arm 18 for the 1st clamp migration which has follower 18a which slides on the inside of cam-groove 19a of a cam 19 in the center section is formed. Moreover, the lower limit of an arm 18 is supported by the frame 9 rotatable by supporting-point 18b, and the upper limit of an arm 18 is supported rotatable by supporting-point 18c prepared in clamp standing-ways 3c of the 1st clamp 3. Therefore, along with 3n of rail members of a linear table, as shown in drawing 8, the 1st clamp 3 moves to the rectangular direction back in the level condition to the shaft of two tubes by rotation of a cam 19, as shown in an arrow head according to the configuration of cam-groove 19a.

[0022] The cutting means 5 has wafer attaching part 5a which holds a wafer exchangeable, arm section 5c in

which wafer attaching part 5a was prepared caudad, follower 5b prepared in the edge of arm section 5c, and 5d of hinge regions and attachment section 5e to a frame 9, as shown in drawing 6. And it can circle to a frame 9 by 5d of hinge regions. And as shown in drawing 6, the temperature detection means 7 for temperature detection of the electrical connection terminal 39 for wafer heating and a wafer is being fixed to the right lateral of the cutting means 5. As a temperature detection means 7, it is desirable that they are a thermocouple or a resistance bulb. More preferably, it is a sheath form thermocouple or a resistance bulb, and a sheath form thermocouple is desirable especially. What has the metal plate bent as a wafer 6 so that it might face each other, the insulating layer formed in the inside of this metal plate, the resistor formed so that the above-mentioned metal plate might not be contacted in this insulating layer, and the terminal for energization prepared in the both ends of this resistor is used suitably.

[0023] And the cam 17 has cam-groove 17a for a cutting means drive in the left lateral, as shown in drawing 6 and drawing 9. And follower 5b of the cutting means 5 is located in cam-groove 17a of a cam 17, and slides on the inside of cam-groove 17a in accordance with the configuration of a cam groove. Therefore, by rotation of a cam 17, as shown in drawing 9, the cutting means 5 will move to a rectangular cross and the perpendicular direction upper and lower sides to the shaft of two tubes, if it puts in another way up and down according to the configuration of cam-groove 17a. Furthermore, the cam 17 has cam-groove 17c for the drive of the 2nd clamp 2 in the center section, as shown in drawing 7. Cam-groove 17c has 17f of left laterals, and right lateral 17e, and controls the location of the 2nd clamp by 17f of left laterals, and right lateral 17e. In 2nd clamp standing-ways 2c, it has the lobe extended caudad, and the follower 20 is formed at the tip. This follower 20 slides on the inside of cam-groove 17c for the drive of the 2nd clamp 2. And between the side faces of a follower 20 and cam-groove 17c, as shown in drawing 7, it is formed so that the clearance between some may be made. And since 2nd clamp standing-ways 2c is always pushed by the spring member 33, in a normal state, a follower 20 comes to contact 17f of left laterals of cam-groove 17c, and the clearance between some is made between a follower 20 and right lateral 17e of cam-groove 17c. However, as mentioned above, if two tubes are held by the 1st and 2nd clamps 3 and 2, since it blockades and two clamps 3 and 2 hold, respectively so that two tubes may be crushed, they will arise [the repulsive force resulting from lock out of a tube]. And in the condition that clamps 3 and 2 hold a tube, since the thing of the force smaller than the repulsive force resulting from lock out of the above-mentioned tube is used, as shown in drawing 7, a follower 20 comes to contact right lateral 17e of cam-groove 17c, and the clearance between some is made by the spring member 33 between a follower 20 and 17f of left laterals of cam-groove 17c. However, since the repulsive force to which a tube originates in cutting **** and lock out of a tube with the above-mentioned cutting means 5 disappears, return and a follower 20 come to contact 17f of left laterals of cam-groove 17c, and the clearance between some is made in a normal state between a follower 20 and right lateral 17e of cam-groove 17c. Thus, it is constituted so that the sliding surface of the cam groove which a follower 20 contacts may change with an operation of the spring member 33 and the repulsive force of a tube with time.

[0024] And as shown in drawing 7, 17d of crevices is formed in 17f of left laterals. Since the stage when a follower 20 passes 17d part of this crevice is after cutting of a tube by the cutting means, a follower 20 is in the condition which meets and is sliding on 17f of left laterals of cam-groove 17c, and, therefore, a follower 20 goes into 17d part of crevices. For this reason, the 2nd clamp 2 will move in the 1st clamp 3 direction by the depth of 17d of crevices. Thereby, junction of a tube becomes more certain. And 17g of crevices is established also in right lateral 17e of cam-groove 17c. 17g of this crevice is a thing for cleaning of the inside of clamps 3 and 2. The 2nd clamp 2 can be moved in the direction estranged from the 1st clamp 3, and, thereby, a clearance is formed between the 1st clamp 3 and the 2nd clamp until a follower 20 contacts 17g of crevices by pushing the 2nd clamp 2 on the spring member 33 side by preparing 17g of this crevice. It becomes possible to clean with the cotton swab containing the solvent which can dissolve the formation ingredient of tubes cut to some extent, such as a cleaning member, for example, alcohol etc., into the formed gap. 17g of this crevice is established in the location which faces mostly 17d (part into which ***** of the 2nd clamp 2 is performed) of crevices of 17f of left laterals, as shown in drawing 7. When the follower 20 formed in the lobe to which 2nd clamp standing-ways 2c is extended caudad is contained in 17d part of crevices, it is in the condition which joined both the tubes made into the purpose after tube cutting, and the 2nd clamp stops in this condition. Moreover, the 1st clamp is also already stopped and the 1st clamp 3 is in the location which shifted from the 2nd clamp. As shown in drawing 1, the 1st clamp 3 is retreating from the 2nd clamp 2, and, specifically, the 1st clamp 3 has it in the location which shifted from the 2nd clamp. For this reason, in this condition, the inside of the point of the 2nd clamp 2 is exposed a little, and has also exposed the inside of the back end section of the 1st clamp a little further. Therefore, the cleaning is easy for

the inside of the 2nd clamp 2 and the 1st clamp 3 which were exposed.

[0025] Next, an operation of the sterile junction equipment 1 of this invention is explained using a drawing. Drawing 11 is a timing chart which shows actuation of a cutting means, the 1st clamp, and the 2nd clamp. Drawing 12, drawing 13, and drawing 14 are the flow charts for explaining an operation of sterile junction equipment. Drawing 15, drawing 16, drawing 17, and drawing 18 are the explanatory views for explaining an operation of sterile junction equipment. With this junction equipment 1, the 1st clamp 3 at the time of junction activity termination serves as a location which shifted from the 2nd clamp 2, and is in the halt location of the timing chart of drawing 11. The include angle of the axis of abscissa of the timing chart of drawing 11 makes 0 degree a zero (condition whose location of the 1st clamp and the 2nd clamp suits), and, in other words, are angle of rotation of the shaft 32 of the subsequent gear 31, and a thing which shows the movement toward the cutting means at the time of angle of rotation of a cam 17 and a cam 19 (wafer), the 1st clamp 3, and the 2nd clamp 2.

[0026] First, as first shown in drawing 12 of a flow chart, the electric power switch prepared in the panel 50 of drawing 3 is pushed. By CPU which constitutes by this the controller 40 shown in drawing 3, when it judges whether it is normal (isn't there any omission of an internal connector, or isn't there specifically any open circuit of a thermocouple, or isn't there any defect in the source of an internal constant voltage?) and is abnormal, a buzzer carries out singing of the junction equipment 1. Then, the clamp reset switch 53 prepared in the panel 50 of drawing 3 is pushed. By CPU, it judges whether the 1st and 2nd clamps are open, whether there are any 1st and 2nd clamps in a zero, and whether a wafer exchange lever is in a zero. In addition, since the clamp used with the sterile junction equipment 1 of this example has lobe 3i to which the 1st clamp 3 projects in the 2nd clamp direction as mentioned above and it has crevice 2i to which the 2nd clamp 2 contains this lobe 3i, the 2nd clamp 2 is constituted so that it cannot blockade, if the 1st clamp 3 is not blockaded. For this reason, it is detected by the microswitch 13 with which ON/OFF of the 1st and 2nd clamps being open is carried out by the lever 16 which contacts, and this lever 16 when the 2nd clamp is blockaded. When the 2nd clamp is in a release condition, OFF has come, when the 2nd clamp 2 is blockaded, a lever 16 is contacted, a lever 16 moves, and, specifically, a microswitch 13 makes a microswitch 13 ON condition. The ON/OFF signal of this microswitch 13 is inputted into a controller 40. It is judged that there are no 1st and 2nd clamps in a zero when a microswitch SW5 (73) and SW6 (74) detect the slot prepared on the periphery of each cam. It is detected by the microswitch 14 that the wafer exchange lever 22 is in a zero. When a microswitch 14 serves as ON when a lever 22 is in a zero, and there is nothing at a zero, OFF comes and the ON/OFF signal of this microswitch 14 is inputted into a controller 40.

[0027] And as shown in drawing 12, when all four above-mentioned points are YES(s), a motor is operated and the 1st and 2nd clamps are returned to a zero. Moreover, an abnormality lamp puts out the light by in No, BUSA's carrying out singing, and an abnormality lamp's lighting up, performing manual discharge, and pushing at least one reset switch among four above-mentioned points. After the 1st and 2nd clamps arrive at a zero, the 1st and 2nd clamps are equipped with two flexible tubes 48 and 49. The 1st and 2nd clamps 3 and 2 in this condition are in the condition that 2f faced mutually slot 3e which is in the condition which both opened wide, and was prepared for both, and 2e and 3f, as [show / in drawing 10]. And the slots 3f and 2f of a near side are equipped with the tube 49 in use, and the slots 3e and 2e by the side of the back are equipped with the intact tube 48 connected. And after blockading the 1st and 2nd clamps 3 and 2 as mentioned above, the wafer exchange lever 22 is pushed on a clamp side, and wafers are exchanged. By lengthening the wafer exchange lever 22 to a clamp side, a wafer newer than the inside of the wafer cartridge 8 is taken out, and while push and a standby wafer are equipped with the used wafer with which push and a standby wafer were equipped with the standby wafer with which the cutting means 5 is equipped with a new wafer by the cutting means 5 in an operating location, a used wafer is contained in the used wafer housing 29. By then, CPU which constitutes the controller 40 which will shift to ** of the flow chart of drawing 13 if the initiation switch of a panel 50 is pushed, and is shown in drawing 3 [whether the 1st and 2nd clamps have closed, whether a wafer is exchange settled, and] Whether the 1st and 2nd clamps are in a zero, whether a wafer exchange lever is in a zero, and whether the 1st and 2nd clamps have closed. When the 2nd clamp is blockaded, it is detected by the lever 16 which contacts, and the microswitch 13 in which ON/OFF is carried out by this lever 16. When the 2nd clamp is in a release condition, OFF has come, when the 2nd clamp 2 is blockaded, a lever 16 is contacted, a lever 16 moves, and, specifically, a microswitch 13 makes a microswitch 13 ON condition. The ON/OFF signal of this microswitch 13 is inputted into a controller 40. If whether a wafer is exchange settled does push and a wafer exchange activity in the clamp direction for the wafer exchange lever 22, since the exchange lever 22 makes a microswitch 15 turn on once, it will be detected whether it was exchanged by ON signal from a microswitch 15. The

ON/OFF signal of a microswitch 15 is inputted into a controller 40. Whether the 1st and 2nd clamps are in a zero detects with a microswitch 13 as mentioned above.

[0028] And as shown in drawing 13, in No, BUSA carries out singing and returns to ** of drawing 12 at least one of the four above-mentioned points. Moreover, when all the four above-mentioned points are YES (s), the working lamp 47 lights up and heating of a wafer is started. It is for or or judging [whose a wafer current is beyond the set point] whether a judgment was made and the wafer has short-circuited this after heating initiation of a wafer. And when a wafer current is not beyond the set point (the electrical potential difference concerning shunt resistance beyond a predetermined value), after waiting for 0.3 seconds, it judges whether a wafer current is set point within the limits. When a wafer is a used thing, since resistance falls for the heat history of a resistor, this measures a wafer current, detects whether it is in a setting range (inside of tolerance) as compared with the wafer current set up beforehand, and, thereby, judges electrically whether a wafer is used. After BUSA carries out singing, suspending heating of a wafer, and the abnormality lamp in a wafer lighting up and pushing a reset switch when the above-mentioned wafer current is beyond the set point, and when an above-mentioned wafer current is not in a setting range (when the wafer has short-circuited) (when a wafer is used), it shifts to flow chart ** of drawing 12. And heating of a wafer is continued when it is in a setting range (inside of tolerance) as compared with a wafer current. Heating of a wafer 6 is performed controlling the source 43 of a constant voltage by the Pulse-Density-Modulation signal computed based on the temperature detection output of the thermocouple 7 which is a wafer temperature detection means. and in order to prevent superfluous heating of a wafer, when it judges whether the heating time of a wafer is predetermined within a time, and it judges whether a wafer current is predetermined value within the limits and beyond the predetermined value, i.e., a wafer, has caused short circuit accident, immediately, BUSA carries out singing, suspends heating of a wafer, and shifts to flow chart ** of drawing 12. And if the temperature of a wafer reaches laying temperature, it shifts to flow chart ** of drawing 14, and a motor operates, thereby, a gear 30, a gear 31, and cams 19 and 17 will rotate, a cutting means (wafer) will go up, and ***** by the side of cutting of a tube, retreat of the 1st clamp, descent of a cutting means (wafer), and the 1st clamp of the 2nd clamp will be performed.

[0029] If it explains concretely, follower 5b of the cutting means 5 will slide on the inside of cam-groove 17a first by rotating in the direction of an arrow head which a cam 17 shows to drawing 9. From the condition that the zero O of a cam groove shown in drawing 9 and drawing 11 at the beginning touched follower 5b, the point A of cam-groove 17a shown in drawing 9 and drawing 11 comes to contact follower 5b. And as shown in drawing 11, gently-sloping, the cutting means 5 goes up and two flexible tubes are cut from the condition that the point A of cam-groove 17a shown in drawing 9 and drawing 11 contacts follower 5b in the meantime, until the point B of cam-groove 17a results in the condition of contacting follower 5b. If it explains using drawing 15 and drawing 16, two tubes 48 and 49 are held by the 1st clamp 3 and the 2nd clamp 2, the tube parts 48a and 49a located between the 1st clamp 3 and the 2nd clamp 2 are formed, and the wafer 6 of a cutting means is located in the lower part. And as mentioned above, by rotation of a cam 17, when the cutting means 5 (wafer 6) goes up, as shown in drawing 16, melting cutting of both is carried out in the tube parts 48a and 49a located between the 1st clamp 3 of two tubes, and the 2nd clamp 2.

[0030] And as shown in drawing 9 and drawing 11, the condition that the cutting means 5 went up is maintained, and the edge from which Tubes 48a and 49a were cut is fully dissolved, until it results in the condition that the point C of cam-groove 17a contacts follower 5b from the condition that the point B of cam-groove 17a shown in drawing 9 contacts follower 5b. And as shown in drawing 9 and drawing 11, the cutting means 5 descends gently-sloping, until the point E of cam-groove 17a results [from the condition that the point C of cam-groove 17a shown in drawing 9 and drawing 11 contacts follower 5b] in the condition of contacting follower 5b. Moreover, as shown in drawing 8, when a cam 19 rotates in the direction of an arrow head, follower 18a prepared in the arm 18 for moving the 1st clamp slides on the inside of cam-groove 19a. From the condition that the zero O of a cam groove shown in drawing 8 and drawing 11 at the beginning touched follower 18a, the point F of cam-groove 19a shown in drawing 8 and drawing 11 comes to contact follower 18a. As shown in the timing chart of drawing 11, follower 18a results in cam-groove 19 a point F early a little rather than follower 5b of the cutting means 5 results in the point B of cam-groove 17a. And as shown in drawing 11, gradually, the 1st clamp 3 retreats, will be in the condition which shows in drawing 17, and will be in the condition that the tube parts 49a and 48a joined faced each other through the wafer 6, until the point G of cam-groove 19a results [from the condition that the point F of cam-groove 19a contacts follower 18a] in the condition of contacting follower 18a, as shown in drawing 8 and drawing 11. As shown in the timing chart of drawing 11, this condition is maintained from the condition that the point G of cam-groove 19a contacts follower 18a until the point C of cam-groove 17a

results in the condition of contacting follower 5b. And the condition of drawing 17 is maintained until the location of the 1st clamp results [from the condition that Point G contacts follower 18a] in the condition that the point H of cam-groove 19a contacts follower 18a. In addition, as the cutting means 5 is shown in drawing 9 and drawing 11 until the point E of cam-groove 17a results [from the condition that the point C of cam-groove 17a shown in drawing 9 and drawing 11 contacts follower 5b as mentioned above] in the condition of contacting follower 5b, it descends gently-sloping and the tube parts 48a and 49a joined contact.

[0031] And with the time of resulting in the condition which descent of the cutting means 5 ended, and the condition that the point E of cam-groove 17a contacts follower 5b, mostly, as shown in drawing 7 and drawing 11, in other words, the 2nd clamp 2 performs ***** to coincidence at the 1st clamp side. As shown in drawing 7 and drawing 11, specifically the point M of 17d of crevices of 17f of left laterals of cam-groove 17c Gradually until the point L of a left lateral results [from the condition of contacting the follower 20 for making the 2nd clamp 2 driving] in the condition of contacting a follower 20 the 2nd clamp 2 It moves to the 1st clamp 3 side, and the condition of having ***** (ed) is maintained until the point K of 17d of crevices results [from the condition that the point L of 17d of crevices of cam-groove 17c contacts a follower 20] in the condition of contacting a follower 20. By this ***** , since both of the tube parts 48a and 49a stick certainly, they can make both junction a more positive thing. And gradually, the 2nd clamp 2 moves in the direction separated from the 1st clamp 3 side, and actuation of a motor stops it in this condition until the point J of 17f of left laterals results [from the condition that the point K of 17d of crevices of cam-groove 17c contacts a follower 20] in the condition of contacting a follower 20.

[0032] Therefore, the location of the 1st clamp 3 and the 2nd clamp 2 in the stopped location is the location shifted like drawing 17, as shown in drawing 18. And if wafer temperature is detected by the thermocouple and wafer temperature becomes below the set point as shown in the flow chart of drawing 14, a run light will put out the light and BUSA will carry out singing. And as shown in drawing 18, the junction activity of a tube is completed by opening the 1st clamp 3 and the 2nd clamp 2, and taking out a tube. Moreover, if it puts in another way until the point C of cam-groove 17a results in the condition of contacting follower 5b, from the condition that the point A of cam-groove 17a shown in drawing 7 and drawing 11 contacts follower 5b, although not indicated to the flow chart of drawing 14 It judges whether as shown in the flow chart of drawing 13, a wafer is laying temperature after the cutting means 5 starts a rise also until it starts descent. It is desirable to control the source 43 of a constant voltage by the Pulse-Density-Modulation signal computed based on the temperature detection output of the thermocouple 7 which is a wafer temperature detection means, and to perform temperature control of a wafer. Since the heat of a wafer is absorbed with a tube and this falls when a wafer contacts the tubes 48 and 49 to cut even if a wafer reaches laying temperature once, it is for performing the amendment. The heating control circuit 55 in drawing 4 especially the temperature detection signal a from the thermocouple which is the temperature detection means 7 as mentioned above The PID amendment machine 56 (proportionality and differential / integral amendment machine 1) of the amendment wafer temperature calculation section 51 amends. The amended amendment temperature signal b shall be outputted and it is the amendment Formula $1b=1-/K-a-(1+K1 \text{ and } T-da/dt) \dots$ By (1), if correction value shall be computed Since the amendment temperature signal b has amended the time lag until the actual temperature of the thermocouple which is a temperature detection signal falls by the fall of the temperature of a wafer in K1 and T-da/dt Since the fall temperature of an actual wafer is detected correctly, temperature control of a wafer can be performed early [correspondence].

[0033]

[Effect of the Invention] The flexible tube sterile junction equipment of this invention is equipment for joining a flexible tube in sterile. This equipment It has a cutting means for cutting said flexible tube between the 1st clamp and the 2nd clamp holding a tube, and this 1st clamp and the 2nd clamp. Said cutting means The source of a constant voltage for heating the wafer and this wafer for carrying out melting cutting of the flexible tube, Having a wafer temperature detection means and a wafer heating control means, said wafer heating control means has the Pulse-Density-Modulation signal output part computed based on the output of said wafer temperature detection means, and controls said source of a constant voltage by this Pulse-Density-Modulation signal. By using the source of a constant voltage, and a Pulse-Density-Modulation signal circuit especially, power consumption can be made small, further, by controlling the source of a constant voltage by the Pulse-Density-Modulation signal, temperature control of a wafer for heating melting to cut a flexible tube can be performed certainly, and a positive tube can be joined.

[Brief Description of the Drawings]

[Drawing 1] Drawing 1 is the perspective view of one example of the flexible tube sterile junction

equipment of this invention.

[Drawing 2] Drawing 2 is the perspective view showing the condition of having contained in the case the sterile junction equipment shown in drawing 1.

[Drawing 3] Drawing 3 is the block diagram showing an example of the electrical circuit used for the sterile junction equipment of this invention, and is **.

[Drawing 4] Drawing 4 is the electrical circuit block diagram showing an example of the wafer heating control means of the electrical circuit of the sterile junction equipment of this invention.

[Drawing 5] Drawing 5 is the plan of one example of the flexible tube sterile junction equipment of this invention.

[Drawing 6] Drawing 6 is the explanatory view of the cutting means used for the flexible tube sterile junction equipment of this invention.

[Drawing 7] Drawing 7 is an explanatory view in order to explain actuation of the 1st clamp, the 2nd clamp, and a cutting means.

[Drawing 8] Drawing 8 is an explanatory view for explaining actuation of the 1st clamp.

[Drawing 9] Drawing 9 is an explanatory view for explaining actuation of a cutting means.

[Drawing 10] Drawing 10 is the perspective view showing an example of the 1st and 2nd clamps used for the sterile junction equipment of this invention.

[Drawing 11] Drawing 11 is a timing chart which shows the timing of the 1st clamp, the 2nd clamp, and a cutting means of operation.

[Drawing 12] Drawing 12 is a flow chart for explaining an operation of the sterile junction equipment of this invention.

[Drawing 13] Drawing 13 is a flow chart for explaining an operation of the sterile junction equipment of this invention.

[Drawing 14] Drawing 14 is a flow chart for explaining an operation of the sterile junction equipment of this invention.

[Drawing 15] Drawing 15 is an explanatory view for explaining an operation of the sterile junction equipment of this invention.

[Drawing 16] Drawing 16 is an explanatory view for explaining an operation of the sterile junction equipment of this invention.

[Drawing 17] Drawing 17 is an explanatory view for explaining an operation of the sterile junction equipment of this invention.

[Drawing 18] Drawing 18 is an explanatory view for explaining an operation of the sterile junction equipment of this invention.

[Drawing 19] Drawing 19 is the schematic diagram of the circuit of the heating means which used the constant current source.

[Drawing 20] Drawing 20 is the schematic diagram of the circuit of the heating means which used the source of a constant voltage.

[Description of Notations]

1 Sterile Junction Equipment

2 2nd Clamp

3 1st Clamp

5 Cutting Means

6 Wafer

7 Wafer Temperature Detection Means

13 Microswitch 1

14 Microswitch 2

15 Microswitch 3

40 Controller

41 Rectification Power Circuit

42 Motor

43 Source of Constant Voltage

44 Wafer Heating Control Means

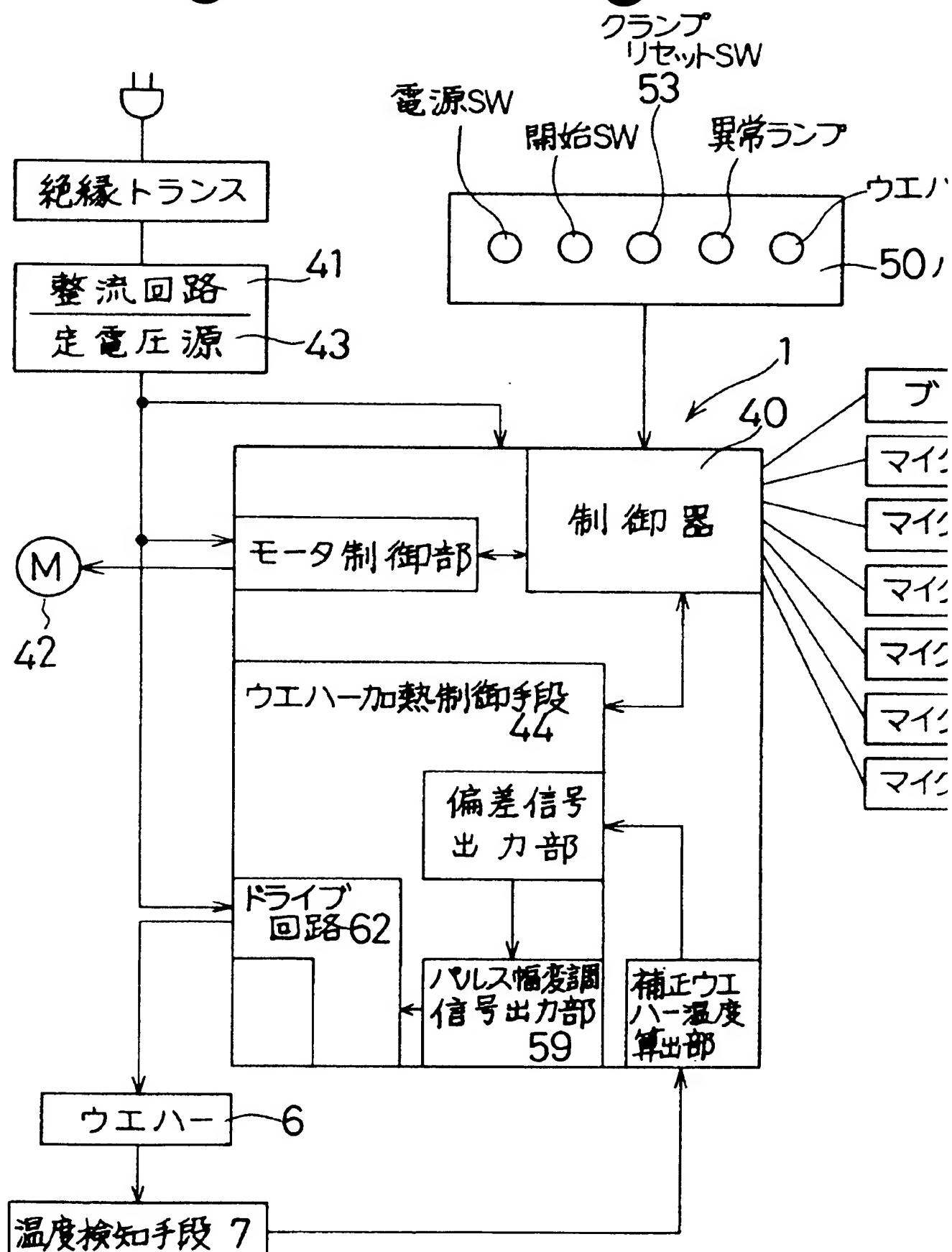
50 Input Panel

59 Pulse-Density-Modulation Signal Output Part

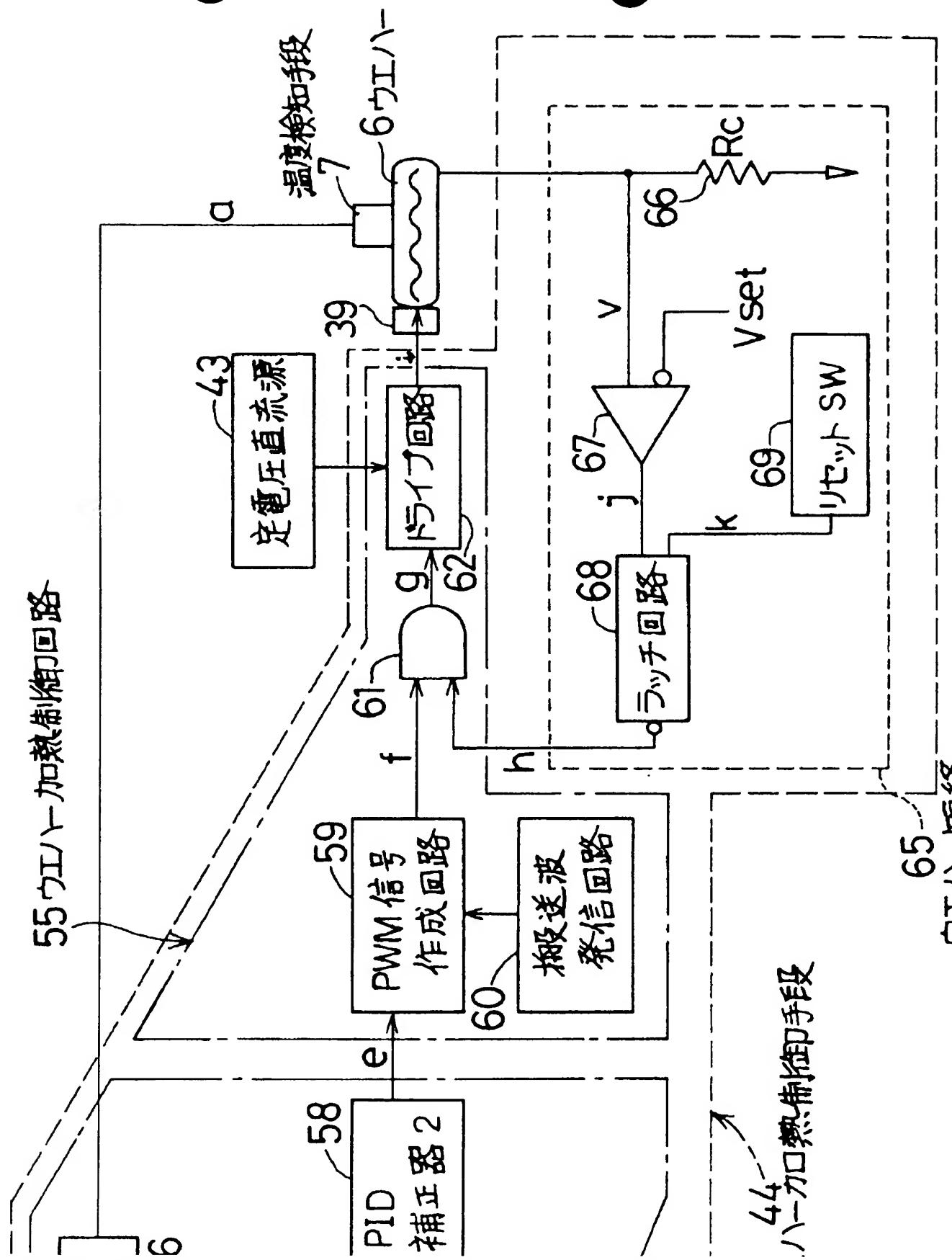
65 Wafer Short Circuit Protection Network

[Procedure amendment 2]

[Document to be Amended] DRAWINGS
[Item(s) to be Amended] drawing 3
[Method of Amendment] Modification
[Proposed Amendment]
[Drawing 3]



[Procedure amendment 3]
[Document to be Amended] DRAWINGS
[Item(s) to be Amended] drawing 4
[Method of Amendment] Modification
[Proposed Amendment]
[Drawing 4]



[Procedure amendment 4]

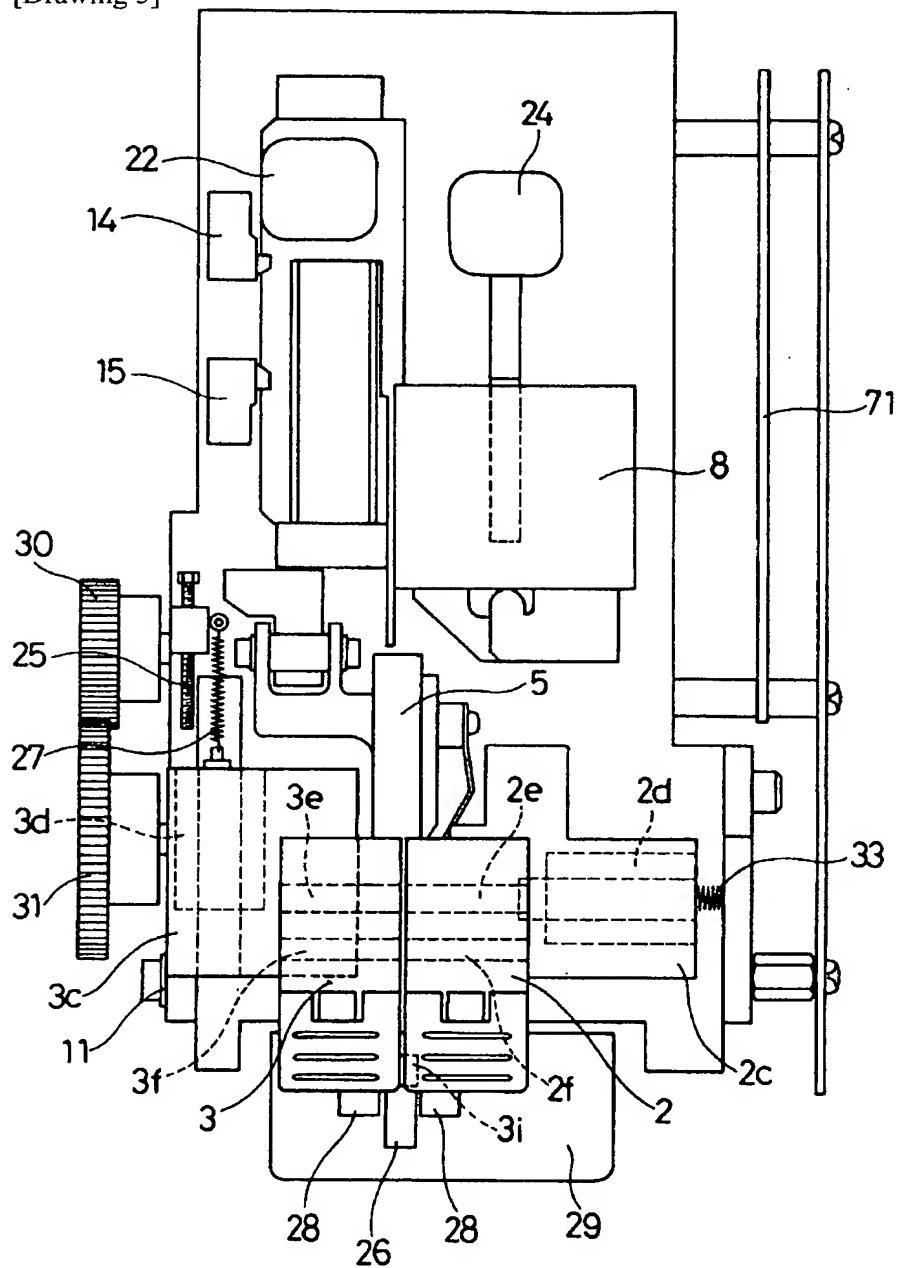
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[Item(s) to be Amended] drawing 5

[Method of Amendment] Modification

[Proposed Amendment]

[Drawing 5]



[Procedure amendment 5]

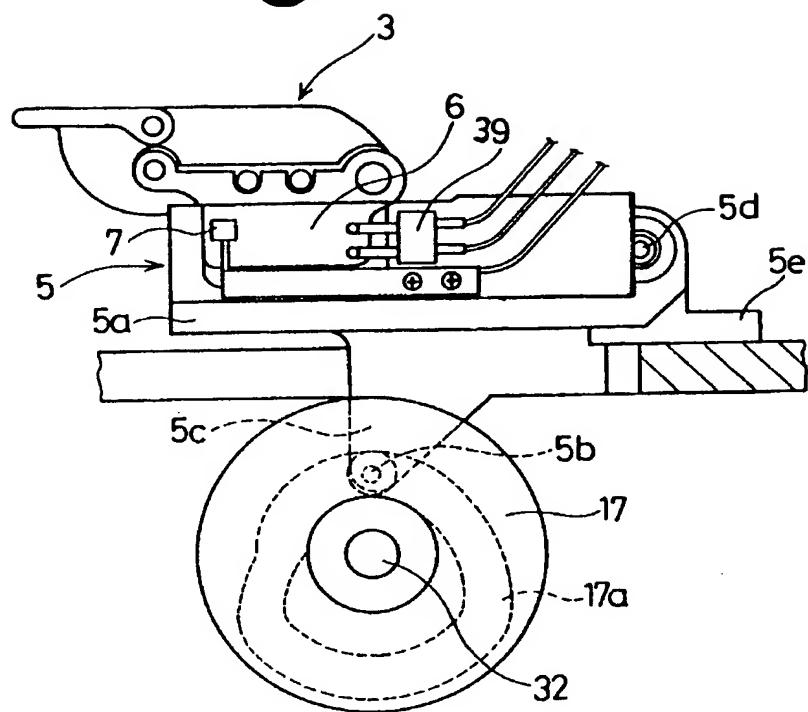
[Document to be Amended] DRAWINGS

[Item(s) to be Amended] drawing 6

[Method of Amendment] Modification

[Proposed Amendment]

[Drawing 6]



[Translation done.]

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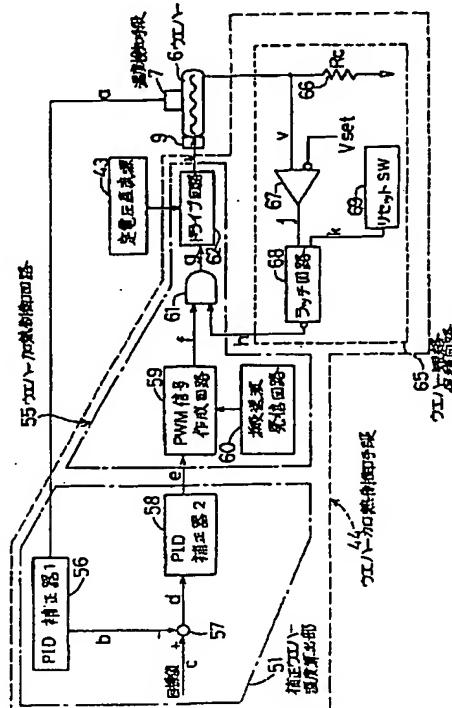
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(54)【発明の名称】可撓性チューブ無菌的接合装置

(57)【要約】

【目的】 可撓性チューブを加熱溶融により切断するためのウェハーの温度制御を確実に行うことができ、さらに、消費電力が少ない可撓性チューブ無菌的接合装置を提供する。

【構成】 少なくとも2本の可撓性チューブを平行状態にて保持する2つのクランプと、2つのクランプ間にてチューブを切断するための切断手段と、切断されたチューブの接合される端部相互が密着するようにいずれかのクランプを移動させる移動手段とを有している。切断手段は、チューブ溶融切断用ウェハーと、ウェハー加熱用定電圧源と、ウェハー温度検知手段と、ウェハー加熱制御手段とを有し、ウェハー加熱制御手段は、温度検知手段の出力に基づいて、算出されるパルス幅変調信号出力部を有し、パルス幅変調信号により定電圧源を制御するものである。



【特許請求の範囲】

【請求項 1】 可撓性チューブを無菌的に接合するための装置であって、該装置は、少なくとも 2 本の可撓性チューブを平行状態にて保持する第 1 クランプおよび第 2 クランプと、該第 1 クランプおよび第 2 クランプ間にて前記可撓性チューブを切断するための切断手段と、該切断手段により切断された可撓性チューブの接合される端部相互が密着するように前記第 1 クランプまたは前記第 2 クランプの少なくとも一方を移動させる移動手段とを有し、前記切断手段は、前記可撓性チューブを溶融切断するためのウエハーと、該ウエハーを加熱するための定電圧源と、ウエハー温度検知手段と、ウエハー加熱制御手段とを有し、前記ウエハー加熱制御手段は、前記ウエハー温度検知手段の出力に基づいて、算出されるパルス幅変調信号出力部を有し、該パルス幅変調信号により前記定電圧源を制御するものであることを特徴とする可撓性チューブ無菌的接合装置。

【発明の詳細な説明】

【0 0 0 1】

【産業上の利用分野】本発明は、少なくとも 2 本の可撓性チューブを加熱溶融して、無菌的に接続するための可撓性チューブ無菌的接合装置に関する。

【0 0 0 2】

【従来の技術】輸血システムにおける採血バッグおよび血液成分バッグのチューブ接続、持続的腹膜透析（C A P D）における透析液バッグと廃液バッグの交換時などには、チューブの接続を無菌的に行うことが必要となる。このようなチューブの無菌的接続を行う装置としては、特公昭 61-30582 号公報に示されものがある。この特公昭 61-30582 号公報に示されている装置は、チューブを加熱溶融して接続するチューブ接続装置であり、接続すべき 2 本の可撓性チューブを平行状態にて保持する第 1 クランプおよび第 2 クランプと、第 1 クランプおよび第 2 クランプ間にて可撓性チューブを切断するための切断手段と、切断手段により切断された可撓性チューブの接合される端部相互が密着するように第 1 クランプまたは第 2 クランプの少なくとも一方を移動させる移動手段とを有している。

【0 0 0 3】 そして、切断手段は、可撓性チューブを溶融切断するためのウエハーと、ウエハーを加熱するための電源とを有している。ウエハーを加熱するための電源としては、特開昭 59-64034 号公報に示されているように、定電流源を用いている。そして、ウエハーの温度制御は、抵抗体の抵抗値温度変化を利用して、抵抗値よりウエハーの温度を予測する方法を用いている。

【0 0 0 4】

【発明が解決しようとする課題】しかし、特開昭 59-64034 号公報に示されているように、定電流源を用い、ウエハーの温度制御は、抵抗体の抵抗値温度変化を利用し、抵抗値よりウエハーの温度を予測する方法で

は、実際にウエハーの温度を測定し制御するものではないので、確実な温度制御を行うことが困難であるという問題点を有している。さらに、定電流源を用いた加熱回路では、駆動回路の損失が大きいため、消費電力が大きいという問題点もあった。そこで、本発明の目的は、可撓性チューブを加熱溶融により切断するためのウエハーの温度制御を確実に行うことができ、さらに、消費電力が少ない可撓性チューブ無菌的接合装置を提供するものである。

10 【0 0 0 5】

【課題を解決するための手段】上記目的を達成するものは、可撓性チューブを無菌的に接合するための装置であって、該装置は、少なくとも 2 本の可撓性チューブを平行状態にて保持する第 1 クランプおよび第 2 クランプと、該第 1 クランプおよび第 2 クランプ間にて前記可撓性チューブを切断するための切断手段と、該切断手段により切断された可撓性チューブの接合される端部相互が密着するように前記第 1 クランプまたは前記第 2 クランプの少なくとも一方を移動させる移動手段とを有し、前記切断手段は、前記可撓性チューブを溶融切断するためのウエハーと、該ウエハーを加熱するための定電圧源と、ウエハー温度検知手段と、ウエハー加熱制御手段とを有し、前記ウエハー加熱制御手段は、前記ウエハー温度検知手段の出力に基づいて、算出されるパルス幅変調信号出力部を有し、該パルス幅変調信号により前記定電圧源を制御するものである可撓性チューブ無菌的接合装置である。

【0 0 0 6】 そして、前記ウエハー加熱制御手段は、前記ウエハー温度検知手段の出力に基づいて、補正ウエハー温度算出部と、該算出部により算出された補正温度と前記ウエハーの目的加熱温度との偏差信号を出力する偏差信号出力部とを有し、前記パルス幅変調信号出力部は、該偏差信号に基づいてパルス幅変調信号を出力するものであることが好ましい。さらに、前記ウエハー加熱制御手段は、ウエハー短絡保護回路を有していることが好ましい。また、前記ウエハー加熱制御手段は、該パルス幅変調信号により前記定電圧源を制御するためのドライブ回路を有しており、前記ウエハー短絡保護回路は、前記ウエハーの短絡検知部と、該短絡検知部の検知信号に基づき、前記パルス幅変調信号出力部からのパルス幅変調信号の前記ドライブ回路への流入を制御するパルス幅変調信号制御部を有していることが好ましい。

また、前記補正ウエハー温度算出部は、比例・積分・微分補正回路を有していることが好ましい。さらに、前記偏差信号出力部は、比例・積分・微分補正回路を有していることが好ましい。そして、前記ウエハー温度検知手段は、熱電対または測温抵抗体であることが好ましい。さらに、前記ウエハー温度検知手段は、シーズ形熱電対または測温抵抗体であることが好ましい。

40 50 【0 0 0 7】 そこで、本発明の可撓性チューブ無菌的接

合装置について、図面を参照して説明する。この可撓性チューブ無菌的接合装置1は、可撓性チューブを無菌的に接合するための装置であって、少なくとも2本の可撓性チューブを平行状態にて保持する第1クランプ3および第2クランプ2と、第1クランプ3および第2クランプ2間に可撓性チューブ48, 49を切断するための切断手段5と、切断手段5により切断された可撓性チューブ48, 49の接合される端部相互48a, 49aが密着するように第1クランプ3または第2クランプ2の少なくとも一方を移動させる移動手段とを有し、切断手段5は、可撓性チューブ48, 49を溶融切断するためのウエハー6と、ウエハー6を加熱するための定電圧源43と、ウエハー温度検知手段7と、ウエハー加熱制御手段44とを有し、ウエハー加熱制御手段44は、ウエハー温度検知手段7の出力に基づいて、算出されるパルス幅変調信号出力部59を有し、パルス幅変調信号により定電圧源43を制御するものである。

【0008】図1は、本発明の可撓性チューブ無菌的接合装置の一実施例の斜視図であり、図2は、図1に示した無菌的接合装置をケースに収納した状態を示す斜視図であり、図3は、本発明の無菌的接合装置に使用される電気回路の一例を示すブロック図であり、図4は、本発明の無菌的接合装置の電気回路のウエハー加熱制御手段の一例を示す電気回路ブロック図である。図5は、本発明の可撓性チューブ無菌的接合装置の一実施例の上面図である。

【0009】次に、図4に記載するウエハー加熱制御手段について説明する。ウエハー6としては、向かい合うように折り曲げられた金属板と、この金属板の内面に形成された絶縁層と、この絶縁層内に上記の金属板と接触しないように形成された抗体と、この抗体の両端部に設けられた通電用端子とを有するものが好適に使用さ

$$b = 1/K \cdot a \cdot (1 + K_1 \cdot T \cdot da/dt) \dots (1)$$

により、補正值を算出する。Kは、ウエハーと熱電対との結合係数であり、K1は、切断される可撓性チューブに起因する補正係数であり、Tは、熱電対の熱時定数である。このような補正を行う目的は、ウエハーと熱電対との間での熱伝導損失に基づく補正(K)を行うこと、熱電対の熱時定数(T)を考慮した補正を行うことにある。そして、式1に示すように、補正温度信号bは、 $1/K$ は定数であるので、実測されたウエハー温度信号aより、ウエハー温度が上昇している間は、 $K_1 \cdot T \cdot da/dt$ 分だけ、高く算出される。熱電対が検知する温度は、熱電対の内部温度であり、ウエハーの表面温度に

$$b(t + \Delta t) = 1/K \cdot a(t + \Delta t) \cdot \{1 + K_1 \cdot T/\Delta t \cdot [a(t + \Delta t) - a(t)]\} \dots (2)$$

このようにして、算出される補正温度信号bは、目標とするウエハー温度信号cと比較され、偏差信号出力部57より偏差信号dが算出される。この偏差信号dは、制御系の応答性を高めるために適当な伝達関数に設計され

れる。そして、抗体は、通電により発熱するため、抗体の発熱は、金属板に伝導されウエハー全体が通電により発熱する。そして、抗体は、通電による発熱により、抵抗値が変化する。よって、定電圧源を単に使用し、ウエハーへの電力供給を調整するだけでは、十分なウエハーの温度制御ができない。そこで、この実施例の無菌的接合装置1では、ウエハー加熱制御手段を有している。

【0010】ウエハー加熱制御手段44は、図4に示すように、ウエハー加熱制御回路55および補正ウエハー温度算出回路51を有しており、さらに、図4に示すようにウエハー短絡保護回路65を有することが好ましい。ウエハー加熱制御回路55は、温度検知手段7からの出力に基づいて、算出されるパルス幅変調信号出力部59を有し、パルス幅変調信号により定電圧源43を制御するものである。具体的には、ウエハー温度検知手段7の出力に基づいて、補正ウエハー温度を算出する補正ウエハー温度算出部56と、算出部により算出された補正温度とウエハーの目的加熱温度との偏差信号を出力する偏差信号出力部57とを有し、パルス幅変調信号出力部59は、偏差信号に基づいてパルス幅変調信号を出力するものである。温度検知手段7としては、熱電対または測温抗体であることが好ましい。より好ましくは、シース形熱電対または測温抗体であり、特に、シース形熱電対が好ましい。

【0011】図4を用いて、加熱制御手段44をより具体的に説明すると、温度検知手段7である熱電対からの温度検知信号aが、補正ウエハー温度算出部56であるPID補正器1(比例・微分・積分補正器1)に入力され、補正された補正温度信号bが出力される。このPID補正器56では、例えば、式1

$$b = 1/K \cdot a \cdot (1 + K_1 \cdot T \cdot da/dt) \dots (1)$$

対して遅れを持っている。しかし、上記の補正を行うことにより、熱電対の遅れを一次遅れに近似して時定数Tとし、補正関数としては、逆に時定数Tの二次進み演算を行うので、ウエハー表面温度を時間遅れなく正確に算出することができる。

【0012】また、式1に示すような補正を行うことにより、ウエハー温度下降時にも、正確なウエハー表面温度を時間遅れなく正確に算出することができる。そして、サンプリングタイム(Δt)を考慮して、式1を書き直すと、式2となる。

たPID補正器2に入力され、補正偏差信号eとして、出力される。この補正偏差信号eは、PWM(パルス幅変調)信号作成回路59に入力される。PWM信号作成回路59は、上記の補正偏差信号eと搬送波発振回路6

0 によって作成される所定周波数に同期し、補正偏差信号 e に比例したパルス幅の信号 (PWM 変調したパルス列信号) f を出力する。このパルス列信号 f は、ゲート回路 6 1 を通り、ドライブ回路 6 2 に流入する。ドライブ回路 6 2 は、半導体スイッチング素子であるトランジスタ、サイリスタなどにより構成されており、入力されたパルス列信号 g は、スイッチング、タイミング信号として作用し、パルス列信号 g が H の状態のときのみ、定電圧源とウエハーが接続される。ドライブ回路 6 2 とウエハー 6 との接続は、接続端子 9 により行われてる。定電圧源 4 3 とウエハー 6 は、パルス列信号 g に基づき断続的に接続され、ウエハーは、目的とするウエハー温度に制御される。

【 0 0 1 3 】 そして、定電流方式の場合の加熱回路の概略は、図 1 9 に示すようになり、定電流方式の加熱回路の損失を求めるとき、損失 (W o) は、

$$W o' = (V i - V o) \cdot I o \text{ であり、}$$

$W o' = [V c e + \{ (V i - V c e) - V o \}] \cdot I o$ (A) となる。また、 PWM 方式の場合の加熱回路の概略は、図 2 0 に示すようになり、駆動回路の損失 (W o) は、

$W o = V o / V i \cdot V c e \cdot I o + W 1$ であり、 (B) $W 1$ は、ドライブ回路を構成するトランジスタのスイッチング損失である。そして、 $W o$ と $W o'$ を比較すると、 B 式において、一般的に次の関係が成り立つ。

$$V o / V i \cdot V c e \cdot I o > W 1$$

次に、 A 式において、一般的に次の関係が成り立つ。

$$V c e \ll (V i - V c e) - V o$$

これにより、 A 式および B 式の第 1 項目、第 2 項目を比較すると、

$$V o / V i \cdot V c e \cdot I o < V c e \cdot I o$$

$$W 1 < (V i - V c e) - V o \cdot I o$$

よって、 $W o < W o'$ となり、 PWM 方式の方が、定電流方式に比べて、消費電力が小さいものである。

【 0 0 1 4 】 次に、ウエハー短絡保護回路について、図 4 を用いて説明する。通常状態においては、コンパレータ 6 7 からの信号 j が、ラッチ回路 6 8 に入力されていないため、ラッチ回路 6 8 は、ゲート回路 6 1 (アンド回路) に対して、常に H の信号を出力している。このため、ゲート回路は、 PWM 信号 f の ON / OFF (H / L) に従って、信号 g をドライブ回路 6 2 に出力する。そして、図 4 に示すように、ウエハー 6 には、シャント抵抗 6 6 が、電気的に接続されており、シャント抵抗 6 6 の電圧 V は、コンパレータ 6 7 により、設定電圧 V set と比較されている。通常状態では、シャント抵抗間の電圧 V は、設定電圧 V set より低いため、コンパレータ 6 7 から信号 j は出力されない。しかし、ウエハー 6 が短絡すると、シャント抵抗 6 6 に規定以上の電流が流れるため、シャント抵抗 6 6 の電圧 V が上昇し、設定電圧 V set より大きくなると、コンパレータ 6 7 から

信号 j が、ラッチ回路 6 8 に出力される。ラッチ回路 6 8 は、一度信号 j が入力されるとその状態を保持する機能を有している。このため、一度信号 j が入力されると、ゲート回路 6 1 (アンド回路) に対して、常に L の信号を出力する。このため、ゲート回路 6 1 からは、 PWM 信号 f に基づく信号 g が、ドライブ回路 6 2 に出力されなくなり、回路が保護される。そして、短絡事故を起こしたウエハーを交換した後、リセットスイッチ 6 9 を押すと、ラッチ回路 6 8 は、ゲート回路 6 1 (アンド回路) に対して、 H の信号を出力する。ラッチ回路 6 8 は、一度リセット信号 k が入力されるとその状態を保持し、通常状態に復帰する。

【 0 0 1 5 】 次に、無菌的接合装置 1 の全体の機構について説明する。この無菌的接合装置 1 は、図 1 、図 2 、図 5 、図 1 0 に示すように、少なくとも 2 本の可撓性チューブを平行状態にて保持する第 1 クランプ 3 および第 2 クランプ 2 を有している。モータの作動により回転するギア 3 0 、ギア 3 0 の回転により回転するギア 3 1 、ギア 3 1 の回転により回転するシャフト 3 2 、シャフト 20 の両端が回転可能に固定されたフレーム 9 、第 1 クランプ 3 の原点位置でのがたつきを防止するための防止部材 1 1 、マイクロスイッチ 1 3 、 1 4 、 1 5 、第 1 クランプ 3 を移動させるための駆動用アーム 1 8 、第 1 クランプ 3 を移動させるためのカム 1 9 、切断手段 5 、切断手段 5 および第 2 クランプ 2 を駆動させるためのカム 1 7 、第 2 クランプ 2 を第 1 クランプ 3 側に押す押圧部材 3 3 、第 1 クランプ 3 の後退位置を規制する規制部材 2 5 、第 1 クランプ 3 のがたつきを防止するためのバネ部材 2 7 、ウエハー交換レバー 2 2 、ウエハーカートリッジ 8 、ウエハーカートリッジ交換レバー 2 4 、使用済ウエハー収納箱把持部材 2 8 、使用済ウエハーを収納箱に誘導するための誘導部材 2 6 、使用済ウエハー収納箱 2 9 、操作パネル 5 0 を有している。

【 0 0 1 6 】 そして、この無菌的接合装置 1 は、切断手段 5 により切断された可撓性チューブ 4 8 、 4 9 の接合される端部相互 4 8 a 、 4 9 a が向かい合うように第 1 クランプ 3 を移動させる第 1 クランプ移動機構と、切断手段 5 をチューブ側に (上方に) 移動させ、切断後再びチューブより離れる方向 (下方に) に移動させるための移動機構と、第 2 クランプ 2 を第 1 クランプ 3 に対して、近接および離間する方向に移動させる第 2 クランプ移動機構とを有している。切断手段駆動機構には、切断手段 5 を 2 本のチューブの軸に対して垂直に上方に移動させ、チューブ切断後下方に移動させるものであり、第 1 クランプ移動機構は、チューブ切断後、第 1 クランプ 3 を 2 本のチューブの軸に対して水平状態にて直交方向 (より具体的には、後方に) に移動させるものであり、第 2 クランプ移動機構は、第 2 クランプ 2 を第 1 クランプ側に近づくように、 2 本のチューブの軸に対して水平状態にてごくわずか平行に移動させるものである。

【0017】そこで、第1および第2クランプ3, 2について説明する。第1および第2クランプ3, 2は、図1、図5、図7および図10に示すように構成されている。具体的には、第1クランプ3は、図10に示すように、ベース3bと、このベース3bに回転可能に取り付けられたカバー3aと、ベース3bが固定されたクランプ固定台3cを有している。そして、このクランプ固定台3cは、リニアテーブルに固定されている。リニアテーブルは、クランプ固定台3cの下面に固定された移動台3cと、移動台3cの下部に設けられたレール部材3nにより構成されている。そして、このリニアテーブルにより、第1クランプ3は、接合するチューブ48, 49の軸に対して垂直方向、言い換えれば、切断された可撓性チューブの接合される端部相互が向かい合うよう、歪みがなく移動する。よって、この実施例の無菌的接合装置1では、第1クランプ移動機構は、上記のリニアテーブル、モータ、ギア30、ギア31、シャフト32、駆動用アーム18、カム19により構成されている。そして、この接合装置1では、図1および図5に示すように、第1クランプ固定台3cの後方と、接合装置1のフレームとを接続するバネ部材27が設けられており、第1クランプ3は、常時後方に引っ張られた状態となっており、第1クランプ3（正確には、第1クランプ固定台3c）のがたつきを少ないものとしている。また、図1、図5に示すように、第1クランプ3のチューブ装着位置（言い換えれば、第1クランプが最も前に出た状態の位置）にて、第1クランプ2のがたつきを防止するための防止部材11が、フレーム9の側面に固定されている。よって、第1クランプ3は、チューブ装着位置では、バネ部材27により後方に引っ張られた状態、つまり、後方側にがたつきがない状態であり、かつ前方をがたつき防止部材により、それより前方に移動できないようになっている。よって、第1クランプ3は、チューブ装着位置では、がたつきがないように構成されている。また、接合装置1には、図1および図5に示すように、第1クランプ3（正確には、第1クランプ固定台3c）の後方の最大移動位置を規制する規制部材25が設けられている。

【0018】第2クランプ2は、図5、図7および図10に示すように、ベース2bと、このベース2bに回転可能に取り付けられたカバー2aと、ベース2bが固定されたクランプ固定台2cを有している。そして、このクランプ固定台2cは、リニアテーブルに固定されている。リニアテーブルは、クランプ固定台2cの下面に固定された移動台2cと、移動台2cの下部に設けられたレール部材2nにより構成されている。そして、このリニアテーブルにより、第2クランプ2は、接合するチューブ48, 49の軸に対して平行な方向、言い換えれば、第2クランプ2を第1クランプ3に対して、近接および離隔する方向にのみ、歪みがなく移動する。

【0019】また、図5および図7に示すように、接合装置1のフレームとクランプ固定台2cとの間には、押圧部材33が設けられており、常時第2クランプ2（正確には、第2クランプ固定台2c）を第1クランプ側に押している。押圧部材としては、バネ部材が好適に使用される。そして、この押圧部材33は、第1および第2クランプ3, 2により2本の可撓性チューブ48, 49を押し潰すようにして把持した時の、可撓性チューブの反発力より押圧部材33の押圧力は弱いものが使用されており、可撓性チューブを把持したとき、第2クランプ2が第1クランプ3より若干は離間する方向に動くように構成されている。よって、この実施例の無菌的接合装置1では、第2クランプ移動機構は、上記のリニアテーブル、モータ、ギア30、ギア31、シャフト32、カム17、押圧部材33により構成されている。

【0020】そして、第1クランプ3および第2クランプ2は、図10に示すように、保持するチューブを斜めに押し潰した状態で保持するように構成されている。クランプ3, 2は、ベース3b, 2bに旋回可能に取り付けられたカバー3a, 2aを有しており、ベース3b, 2bには、2つのチューブを裁置するために平行に設けられた2つのスロット3f, 3eおよび2f, 2eを有している。そして、スロット3f, 3eとスロット2f, 2eが向かい合う部分のベース3b, 2bの端面には、鋸刃状の閉塞部材3h, 2hが設けられている。そして、カバー3a, 2aには、上記のベース3b, 2bの閉塞部材3h, 2hに対応する形状の鋸刃状の閉塞部材3g, 2gが設けられている。カバー3a, 2aの内表面は平坦となっている。そして、カバー3a, 2aには、それぞれ旋回カムを有しており、この旋回カムは、カバー3a, 2aを閉じると、ベース3b, 2bのローラと係合する。そして、2本のチューブは、カバー3a, 2aが閉じられたとき、ベース3bの閉塞部材3hとカバー3aの閉塞部材3gとの間、およびベース2bの閉塞部材2hとカバー2aの閉塞部材2gとの間により、斜めに押し潰され、閉塞した状態で保持される。また、第1クランプ3は、第2クランプ方向に突出する突出部3iを有し、第2クランプ2が、この突出部3iを収納する凹部2iを有しているので、第2クランプ2は、第1クランプ1を閉塞しないと、閉塞できないように構成されている。

【0021】そして、無菌的接合装置1は、図1に示すように、モータにより回転するギア30と、このギア30の回転により回転するギア31を有しており、ギア31のシャフト32には、図7に示すように、2つのカム19, 17が固定されており、カム19, 17は、ギア31の回転と共に回転する。そして、カム19の右側面には、図8に示すような形状の第1クランプ駆動用のカム溝19aが設けられている。そして、カム19のカム溝19a内を摺動するフォロア18aを中央部に有する

第1クランプ移動用アーム18が設けられている。また、アーム18の下端は、支点18bによりフレーム9に回動可能に支持されており、アーム18の上端は、第1クランプ3のクランプ固定台3cに設けられた支点18cにより回動可能に支持されている。よって、第1クランプ3は、リニアテーブルのレール部材3nに沿って、図8に示すように、カム19の回転により、カム溝19aの形状に従い矢印に示すように、2本のチューブの軸に対して水平状態にて直交方向後方に移動する。

【0022】切断手段5は、図6に示すように、ウエハーを交換可能に保持するウエハー保持部5aと、ウエハー保持部5aの下方に設けられたアーム部5cと、アーム部5cの端部に設けられたフォロア5bと、ヒンジ部5dと、フレーム9への取付部5eを有している。そして、ヒンジ部5dによりフレーム9に対して旋回可能となっている。そして、図6に示すように、切断手段5の右側面には、ウエハー加熱用の電気接続端子9、ウエハーの温度検知のための温度検知手段7が固定されている。温度検知手段7としては、熱電対または測温抵抗体であることが好ましい。より好ましくは、シース形熱電対または測温抵抗体であるり、特に、シース形熱電対が好ましい。ウエハー6としては、向かい合うように折り曲げられた金属板と、この金属板の内面に形成された絶縁層と、この絶縁層内に上記の金属板と接触しないように形成された抵抗体と、この抵抗体の両端部に設けられた通電用端子とを有するものが好適に使用される。

【0023】そして、カム17は、図6および図9に示すように、左側面に切断手段駆動用のカム溝17aを有している。そして、切断手段5のフォロア5bは、カム17のカム溝17a内に位置しており、カム溝17a内をカム溝の形状に沿って摺動する。よって、切断手段5は、図9に示すように、カム17の回転により、カム溝17aの形状に従い上下に、言い換えれば、2本のチューブの軸に対して、直交かつ垂直方向上下に移動する。さらに、カム17は、図7に示すように、中央部に第2クランプ2の駆動用のカム溝17cを有している。カム溝17cは、左側面17fおよび右側面17eを有しており、左側面17fおよび右側面17eにより、第2クランプの位置を制御する。第2クランプ固定台2cには下方にのびる突出部を有しており、その先端にはフォロア20が設けられている。このフォロア20は、第2クランプ2の駆動用のカム溝17c内を摺動する。そして、図7に示すように、フォロア20とカム溝17cの側面間には、若干の隙間ができるように形成されている。そして、第2クランプ固定台2cは、バネ部材33により常に押されているため、通常状態では、フォロア20は、カム溝17cの左側面17fに当接するようになり、フォロア20とカム溝17cの右側面17eとの間に若干の隙間ができる。しかし、第1および第2クランプ3, 2により2本のチューブを保持すると、上述の

ように、2つのクランプ3, 2はそれぞれ、2本のチューブを押し潰すように閉塞し保持するため、チューブの閉塞に起因する反発力が生ずる。そして、バネ部材33は、上記チューブの閉塞に起因する反発力より小さい力のものが用いられているため、クランプ3, 2がチューブを保持する状態では、図7に示すように、フォロア20は、カム溝17cの右側面17eに当接するようになり、フォロア20とカム溝17cの左側面17fとの間に若干の隙間ができる。しかし、上述の切断手段5によりチューブが切斷されると、チューブの閉塞に起因する反発力が消失するため、通常状態に戻り、フォロア20は、カム溝17cの左側面17fに当接するようになり、フォロア20とカム溝17cの右側面17eとの間に若干の隙間ができる。このように、バネ部材33の作用およびチューブの反発力により、フォロア20が当接するカム溝の摺動面が経時的に変化するように構成されている。

【0024】そして、図7に示すように、左側面17fに凹部17dが形成されている。この凹部17d部分をフォロア20が通過する時期は、切断手段によりチューブの切断後であるため、フォロア20は、カム溝17の左側面17fを沿って摺動している状態であり、よって、フォロア20は凹部17d部分に入る。このため、凹部17dの深さ分だけ、第2クランプ2が第1クランプ3方向に移動することになる。これにより、チューブの接合がより確実となる。そして、カム溝17cの右側面17eにも凹部17gが設けられている。この凹部17gは、クランプ3, 2の内面の清掃のためのものである。この凹部17gを設けることにより、第2クランプ2をバネ部材33側に押すことにより、フォロア20が凹部17gに当接するまで、第2クランプ2を第1クランプ3より離間する方向に移動することができ、これにより、第1クランプ3と第2クランプとの間に隙間が形成される。形成された隙間に内に清掃部材、例えば、アルコールなどのある程度切斷されるチューブの形成材料を溶解できる溶剤を含有した綿棒により清掃することができる。この凹部17gは、図7に示すように、左側面17fの凹部17d（第2クランプ2の幅寄せが行われる部分）とほぼ向かい合う位置に設けられている。第40 2クランプ固定台2cの下方にのびる突出部に設けられたフォロア20が凹部17d部分に入っているときは、チューブ切斷後、目的とするチューブ相互を接合した状態であり、この状態にて、第2クランプは停止する。また、第1クランプも既に停止しており、かつ、第1クランプ3は、第2クランプとずれた位置にある。具体的には、図1に示すように、第1クランプ3が、第2クランプ2より後退しており、第1クランプ3は、第2クランプとずれた位置にある。このため、この状態では、第2クランプ2の先端部の内面が若干露出しており、さらに、第1クランプの後端部の内面も若干露出している。

よって、露出した第2クランプ2の内面および第1クランプ3は、その清掃が容易である。

【0025】次に、本発明の無菌的接合装置1の作用を図面を用いて説明する。図11は、切断手段、第1クランプ、第2クランプの動作を示すタイミングチャートである。図12、図13および図14は、無菌的接合装置の作用を説明するためのフローチャートである。図15、図16、図17および図18は、無菌的接合装置の作用を説明するための説明図である。この接合装置1では、接合作業終了時の第1クランプ3は、第2クランプ2と離れた位置となっており、図11のタイミングチャートの停止位置にある。図11のタイミングチャートの横軸の角度は、原点(第1クランプと第2クランプの位置があつてある状態)を0°とし、その後のギア31のシャフト32の回転角度、言い換えれば、カム17およびカム19の回転角度のときの、切断手段(ウエハ一)、第1クランプ3、第2クランプ2の動きを示すものである。

【0026】まず、最初にフローチャートの図12に示すように、図3のパネル50に設けられている電源スイッチ51を押す。これにより、図3に示す制御器40を構成するCPUにより、接合装置1は、異常が無いか(具体的には、内部コネクタの抜けがないか、熱電対の断線がないか、内部定電圧源に不良がないか)を判断し、以上がある場合は、ブザーが鳴動する。続いて、図3のパネル50に設けられているクランプリセッットスイッチ53を押す。CPUにより、第1および第2クランプが開いているか否か、第1および第2クランプが原点にないか否か、ウエハ交換レバーが原点にあるか否かを判断する。なお、この実施例の無菌的接合装置1で使用するクランプは、上述のように、第1クランプ3が、第2クランプ方向に突出する突出部3iを有し、第2クランプ2が、この突出部3iを収納する凹部2iを有しているので、第2クランプ2は、第1クランプ1を閉塞しないと、閉塞できないように構成されている。このため、第1および第2クランプが開いていることは、第2クランプが閉塞されたときに、接触するレバー16と、このレバー16によりON/OFFされるマイクロスイッチ13により検知される。具体的には、マイクロスイッチ13は、第2クランプが解放状態のときは、OFFとなっており、第2クランプ2が閉塞されたときにレバー16と接触し、レバー16が動きマイクロスイッチ13をON状態とする。このマイクロスイッチ13のON/OFF信号は、制御器40に入力される。第1および第2クランプが原点にないことは、それぞれのカムの円周上に設けられた溝をマイクロスイッチSW5(73)、SW6(74)が検知することにより判断される。ウエハ交換レバー22が原点にあることは、マイクロスイッチ14により検知される。レバー22が、原点にある場合は、マイクロスイッチ14がONとなり、原点にな

い場合は、OFFとなり、このマイクロスイッチ14のON/OFF信号は、制御器40に入力される。

【0027】そして、図12に示すように、上述の4つの点すべてがYESの場合、モータを作動させ、第1および第2クランプを原点に復帰させる。また、上述の4つの点のうちいずれか1つでもNOの場合、ブザーが鳴動し、異常ランプが点灯し、手動解除を行い、リセットスイッチを押すことにより、異常ランプが消灯する。第1および第2クランプが原点に到達した後、2本の可撓性チューブ48、49を第1および第2クランプに装着する。この状態での第1および第2クランプ3、2は、図10に示すように、両者とも開放した状態であり、かつ両者に設けられたスロット3eと2eおよび3fと2fは互いに向かいあつた状態となっている。そして、使用中のチューブ49を手前側のスロット3f、2fに装着し、接続される未使用のチューブ48を奥側のスロット3e、2eに装着する。そして、上記のように第1および第2クランプ3を閉塞した後、ウエハ交換レバー22をクランプ側に押して、ウエハを交換する。ウエハ交換レバー22をクランプ側に押すことにより、ウエハーカートリッジ8内より、新しいウエハが取り出され、新しいウエハが、切断手段5に装着されている待機ウエハを押し、待機ウエハが切断手段5に装着されていた使用済ウエハを押し、待機ウエハが使用位置に装着されるとともに、使用済ウエハは、使用済ウエハ収納箱29内に収納される。続いて、パネル50の開始スイッチ52を押すと図13のフローチャートの②に移行し、図3に示す制御器40を構成するCPUにより、第1および第2クランプが閉じているか否か、ウエハが交換済であるか否か、第1および第2クランプが原点にあるか否か、ウエハ交換レバーが原点にあるか否か、第1および第2クランプが閉じているか否かは、第2クランプが閉塞されたときに、接触するレバー16と、このレバー16によりON/OFFされるマイクロスイッチ13により検知される。具体的には、マイクロスイッチ13は、第2クランプが解放状態のときは、OFFとなっており、第2クランプ2が閉塞されたときにレバー16と接触し、レバー16が動き、マイクロスイッチ13をON状態とする。このマイクロスイッチ13のON/OFF信号は、制御器40に入力される。ウエハが交換済であるか否かは、ウエハ交換レバー22をクランプ方向に押し、ウエハ交換操作業を行うと、交換レバー22は、マイクロスイッチ15を一度ONさせるので、マイクロスイッチ15からのON信号により交換されたか否か検知される。マイクロスイッチ15のON/OFF信号は、制御器40に入力される。第1および第2クランプが原点にあるか否かは、上述のようにマイクロスイッチ5、6により検知する。

【0028】そして、図13に示すように、上述の4つの点のいずれか1つでもNOの場合、ブザーが鳴動し、

図 12 の③にもどる。また、上述の 4 つの点のすべてが YES の場合、動作中ランプ 47 が点灯し、ウェハーの加熱が開始される。ウェハーの加熱開始後、ウェハー電流が設定値以上であるか判断し、これは、ウェハーが短絡しているかを判断するためである。そして、ウェハー電流が設定値以下（シャント抵抗にかかる電圧が所定値以上）でない場合は、0.3 秒待った後に、ウェハー電流が設定値範囲内であるか判断する。これは、ウェハーが使用済のものである場合、抵抗体の熱履歴のために、抵抗値が低下するため、ウェハー電流を測定し、あらかじめ設定したウェハー電流と比較し、設定範囲内（許容範囲内）であるかを検知し、これにより、ウェハーが使用済であるかを電気的に判断する。上記のウェハー電流が設定値以上である場合（ウェハーが短絡している場合）および、上述のウェハー電流が設定範囲内でない場合（ウェハーが使用済みの場合）は、ブサーが鳴動し、ウェハーの加熱を停止し、ウェハー異常ランプが点灯し、リセットスイッチが押された後、図 12 のフローチャート⑤に移行する。そして、ウェハー電流と比較し、設定範囲内（許容範囲内）である場合は、ウェハーの加熱が継続される。ウェハー 6 の加熱は、ウェハー温度検知手段である熱電対 7 の温度検知出力に基づいて、算出されるパルス幅変調信号により定電圧源 43 を制御しながら行われる。そして、ウェハーの過剰加熱を防止するために、ウェハーの加熱時間が所定時間内であるか判断し、また、ウェハー電流が所定値以下であるか判断し、所定値以下、つまりウェハーが短絡事故を起こしている場合は、直ちにブサーが鳴動し、ウェハーの加熱を停止し、図 12 のフローチャート⑤に移行する。そして、ウェハーの温度が設定温度に達すると、図 14 のフローチャート④に移行し、モータが作動し、これにより、ギア 30、ギア 31、カム 19、17 が回転し、切断手段（ウェハー）の上昇し、チューブの切断、第 1 クランプの後退、切断手段（ウェハー）の下降、第 2 クランプの第 1 クランプ側への幅寄せが行われる。

【0029】具体的に説明すると、まず、カム 17 が矢印方向に回転することにより、切断手段 5 のフォロア 5b は、カム溝 17a 内を摺動をする。当初図 9 および図 11 に示すカム溝の原点 O がフォロア 5b と接触していた状態より、図 9 および図 11 に示すカム溝 17a の点 A がフォロア 5b と接触するようになる。そして、図 9 および図 11 に示すカム溝 17a の点 A がフォロア 5b と接触する状態から、カム溝 17a の点 B がフォロア 5b と接触する状態に至るまでの間、図 11 に示すように、なだらかに切断手段 5 は上昇し、この間において、2 本の可撓性チューブが切断される。図 15 および図 16 を用いて説明すると、2 本のチューブ 48、49 は、第 1 クランプ 3 および第 2 クランプ 2 により保持されており、第 1 クランプ 3 および第 2 クランプ 2 の間に位置するチューブ部分 48a、49a が形成され、その下方

に切断手段のウェハー 6 が位置している。そして、上述のように、カム 17 の回転により、切断手段 5（ウェハー 6）が上昇することにより、図 16 に示すように、2 本のチューブの第 1 クランプ 3 および第 2 クランプ 2 の間に位置するチューブ部分 48a、49a にて両者を溶融切断する。

【0030】そして、図 9 に示すカム溝 17a の点 B がフォロア 5b と接触する状態から、カム溝 17a の点 C がフォロア 5b と接触する状態に至るまでの間、図 9 および図 11 に示すように、切断手段 5 は、上昇した状態が維持され、チューブ 48a、49a の切断された端部を十分に溶解する。そして、図 9 および図 11 に示すカム溝 17a の点 C がフォロア 5b と接触する状態から、カム溝 17a の点 E がフォロア 5b と接触する状態に至るまでの間、図 9 および図 11 に示すように、なだらかに切断手段 5 は下降する。また、図 8 に示すように、カム 19 が矢印方向に回転することにより、第 1 クランプを移動させるためのアーム 18 に設けられたフォロア 18a は、カム溝 19a 内を摺動をする。当初図 8 および図 11 に示すカム溝の原点 O がフォロア 18a と接触していた状態より、図 8 および図 11 に示すカム溝 19a の点 F がフォロア 18a と接触するようになる。図 11 のタイミングチャートに示すように、切断手段 5 のフォロア 5b がカム溝 17a の点 B に至るより若干早く、フォロア 18a は、カム溝 19a 点 F に至る。そして、図 8 および図 11 に示すように、カム溝 19a の点 F がフォロア 18a と接触する状態から、カム溝 19a の点 G がフォロア 18a と接触する状態に至るまでの間、図 11 に示すように、徐々に第 1 クランプ 3 は後退し、図 17 に示す状態となり、接合されるチューブ部分 49a と 48a がウェハー 6 を介して向かい合った状態となる。この状態は、図 11 のタイミングチャートに示すように、カム溝 19a の点 G がフォロア 18a と接触する状態から、カム溝 17a の点 C がフォロア 5b と接触する状態に至るまでの間維持される。そして、第 1 クランプの位置は、点 G がフォロア 18a と接触する状態から、カム溝 19a の点 H がフォロア 18a と接触する状態に至るまでの間、図 17 の状態が維持される。なお、切断手段 5 は、上述のように、図 9 および図 11 に示すカム溝 17a の点 C がフォロア 5b と接触する状態から、カム溝 17a の点 E がフォロア 5b と接触する状態に至るまでの間、図 9 および図 11 に示すように、なだらかに下降し、接合されるチューブ部分 48a、49a が当接する。

【0031】そして、切断手段 5 の下降が終了した状態、言い換えれば、カム溝 17a の点 E がフォロア 5b と接触する状態に至ったときとほぼ同時に、図 7 および図 11 に示すように、第 2 クランプ 2 が、第 1 クランプ側に幅寄せを行う。具体的には、図 7 および図 11 に示すように、カム溝 17c の左側面 17d の点 N が、第 2

クランプ2を駆動させるためのフォロア20と接触する状態から、左側面の点Lがフォロア20と接触する状態に至るまでの間、徐々に、第2クランプ2は、第1クランプ3側に移動し、カム溝17cの凹部17dの点LKが、フォロア20と接触する状態から、凹部17dの点Kがフォロア20と接触する状態に至るまでの間、幅寄せした状態を維持する。この幅寄せにより、チューブ部分48a、49aの両者は確実に密着するので、両者の接合をより確実なものとにすることができる。そして、カム溝17cの凹部17dの点Kが、フォロア20と接触する状態から、左側面17fの点Jがフォロア20と接触する状態に至るまでの間、徐々に、第2クランプ2は、第1クランプ3側より離れる方向に移動し、この状態で、モータの作動が停止する。

【0032】よって、停止した位置での、第1クランプ3は、第2クランプ2の位置は、図18に示すように、図17と同様にずれた位置となっている。そして、図14のフローチャートに示すように、熱電対によりウエハー温度が検知され、ウエハー温度が設定値以下になると、動作ランプが消灯し、ブサーが鳴動する。そして、図18に示すように、第1クランプ2および第2クラン

$$b = 1/K \cdot a \cdot (1 + K_1 \cdot T \cdot da/dt) \dots (1)$$

により、補正值を算出するものとすると、補正温度信号bは、ウエハーの温度の低下によって、温度検知信号である熱電対の実際の温度が低下するまでの時間遅れを、 $K_1 \cdot T \cdot da/dt$ にて補正しているので、実際のウエハーの低下温度を正確に検知するので、対応早く、ウエハーの温度制御を行うことができる。

【0033】

【発明の効果】本発明の可撓性チューブ無菌的接合装置は、可撓性チューブを無菌的に接合するための装置であって、該装置は、少なくとも2本の可撓性チューブを平行状態にて保持する第1クランプおよび第2クランプと、該第1クランプおよび第2クランプ間にて前記可撓性チューブを切断するための切断手段と、該切断手段により切断された可撓性チューブの接合される端部相互が密着するように前記第1クランプまたは前記第2クランプの少なくとも一方を移動させる移動手段とを有し、前記切断手段は、前記可撓性チューブを溶融切断するためのウエハーと、該ウエハーを加熱するための定電圧源と、ウエハー温度検知手段と、ウエハー加熱制御手段とを有し、前記ウエハー加熱制御手段は、前記ウエハー温度検知手段の出力に基づいて、算出されるパルス幅変調信号出力部を有し、該パルス幅変調信号により前記定電圧源を制御するものである。特に、定電圧源とパルス幅変調信号回路を用いることにより、消費電力を小さいものとすることができます、さらに、パルス幅変調信号により定電圧源を制御することにより、可撓性チューブを加熱溶融により切断するためのウエハーの温度制御を確実に行うことができ、確実なチューブの接合を行うことができ

る。また、図14のフローチャートには記載していないが、図7および図11に示すカム溝17aの点Aがフォロア5bと接触する状態より、カム溝17aの点Cがフォロア5bと接触する状態に至るまでの間、言い換えれば、切断手段5が上昇を開始してから下降を開始するまでの間も、図13のフローチャートに示すようにウエハーが設定温度であるかを判断し、ウエハー温度検知手段である熱電対7の温度検知出力に基づいて、算出されるパルス幅変調信号により定電圧源43を制御し、ウエハーの温度制御を行うことが好ましい。これは、一度ウエハーが設定温度に到達しても、切断するチューブ48、49にウエハーが接触することにより、ウエハーの熱がチューブにより吸収され低下するため、その補償を行うためである。特に、上述のように、図4における加熱制御回路55が、温度検知手段7である熱電対からの温度検知信号aを、補正ウエハー温度算出部56であるPID補正器56（比例・微分・積分補正器1）により補正し、補正した補正温度信号bを出力するものとし、その補正を式1

きる。

【図面の簡単な説明】

【図1】図1は、本発明の可撓性チューブ無菌的接合装置の一実施例の斜視図である。

【図2】図2は、図1に示した無菌的接合装置をケースに収納した状態を示す斜視図である。

【図3】図3は、本発明の無菌的接合装置に使用される電気回路の一例を示すブロック図である

【図4】図4は、本発明の無菌的接合装置の電気回路のウエハー加熱制御手段の一例を示す電気回路ブロック図である。

【図5】図5は、本発明の可撓性チューブ無菌的接合装置の一実施例の上面図である。

【図6】図6は、本発明の可撓性チューブ無菌的接合装置に使用される切断手段の説明図である。

【図7】図7は、第1クランプ、第2クランプおよび切断手段の動作を説明するために説明図である。

【図8】図8は、第1クランプの動作を説明するための説明図である

【図9】図9は、切断手段の動作を説明するための説明図である。

【図10】図10は、本発明の無菌的接合装置に使用される第1および第2クランプの一例を示す斜視図である。

【図11】図11は、第1クランプ、第2クランプおよび切断手段の動作タイミングを示すタイミングチャートである。

【図12】図12は、本発明の無菌的接合装置の作用を

説明するためのフローチャートである。

【図 1 3】図 1 3 は、本発明の無菌的接合装置の作用を説明するためのフローチャートである。

【図 1 4】図 1 4 は、本発明の無菌的接合装置の作用を説明するためのフローチャートである。

【図 1 5】図 1 5 は、本発明の無菌的接合装置の作用を説明するための説明図である。

【図 1 6】図 1 6 は、本発明の無菌的接合装置の作用を説明するための説明図である。

【図 1 7】図 1 7 は、本発明の無菌的接合装置の作用を説明するための説明図である。

【図 1 8】図 1 8 は、本発明の無菌的接合装置の作用を説明するための説明図である。

【図 1 9】図 1 9 は、定電流源を用いた加熱手段の回路の概略図である。

【図 2 0】図 2 0 は、定電圧源を用いた加熱手段の回路の概略図である。

【符号の説明】

1 無菌的接合装置

2 第2クランプ

3 第1クランプ

5 切断手段

6 ウエバー

7 ウエバー温度検知手段

13 マイクロスイッチ 1

14 マイクロスイッチ 2

15 マイクロスイッチ 3

10 40 制御器

41 整流電源回路

42 モーター

43 定電圧源

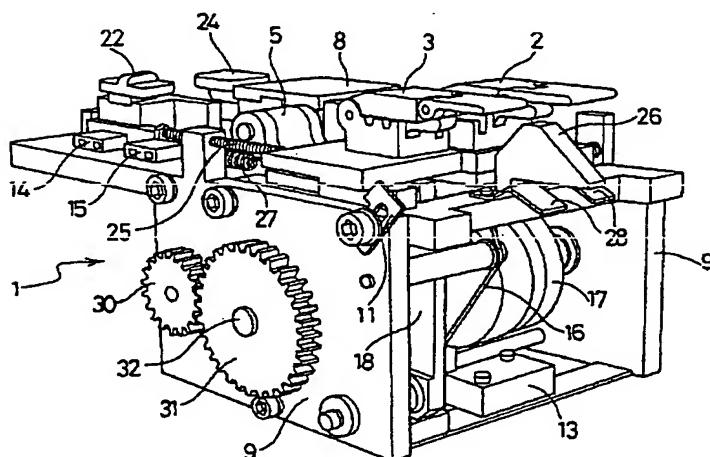
44 ウエバー加熱制御手段

50 入力パネル

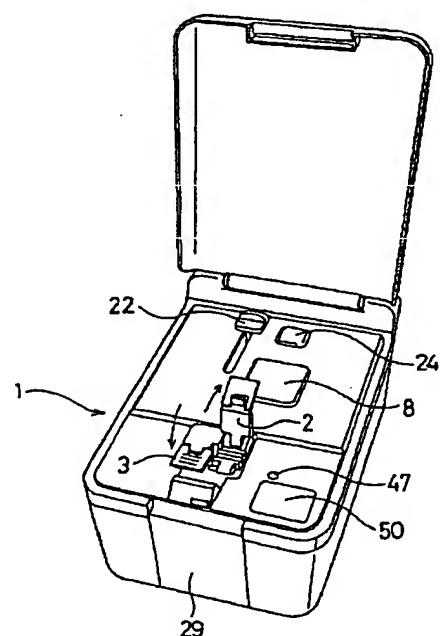
59 パルス幅変調信号出力部

65 ウエバー短絡保護回路

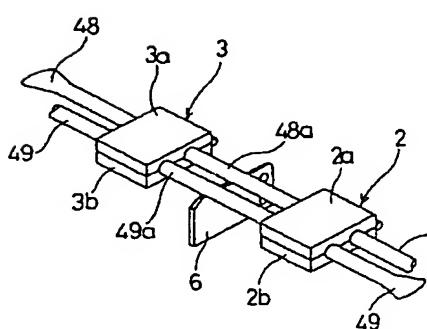
【図 1】



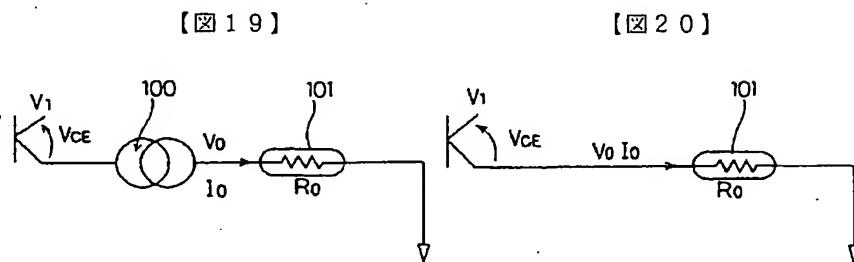
【図 2】



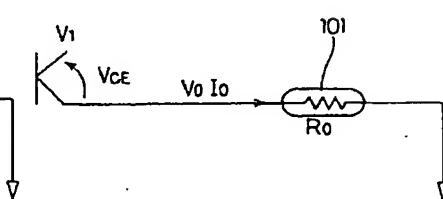
【図 1 5】



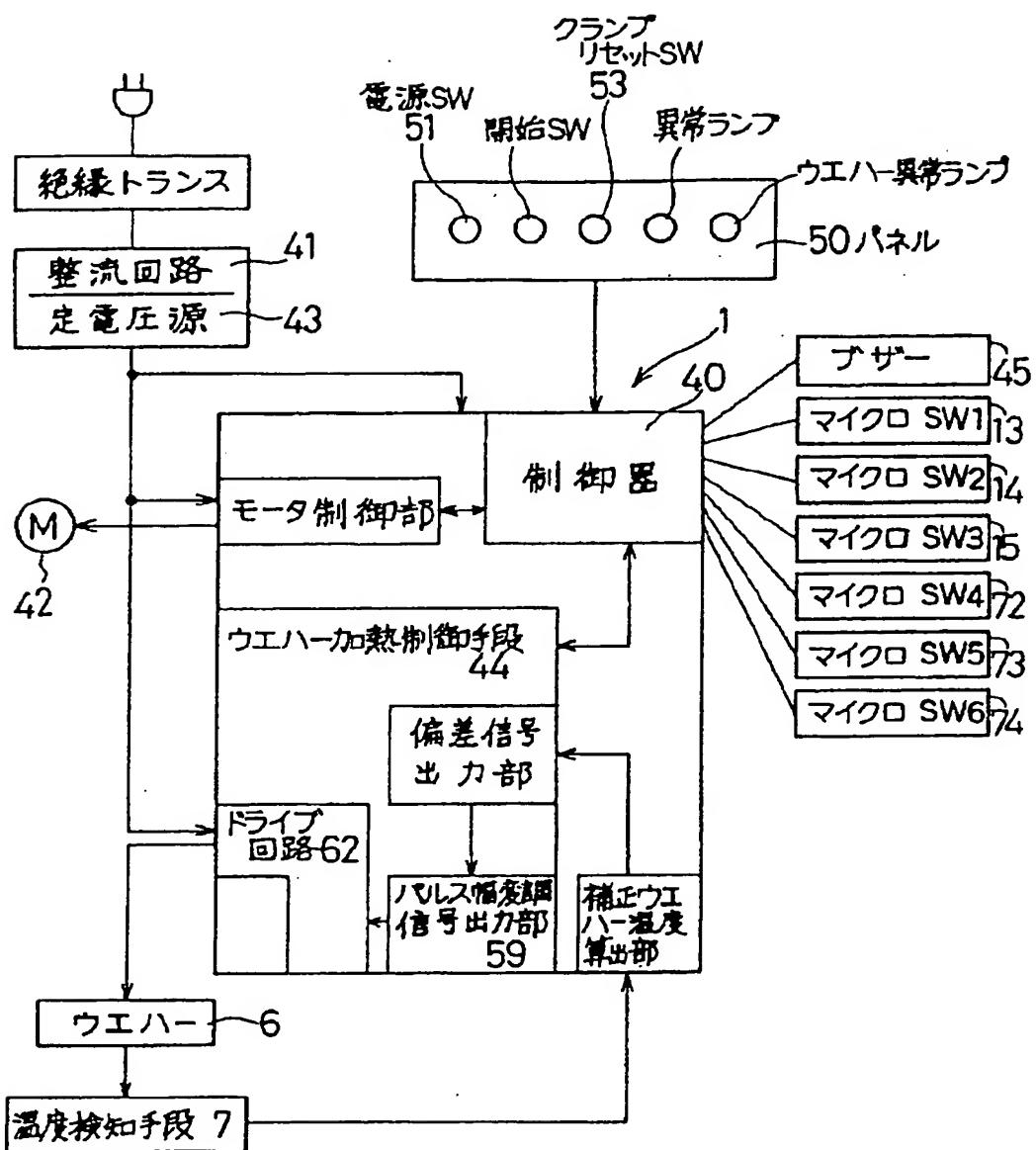
【図 1 9】



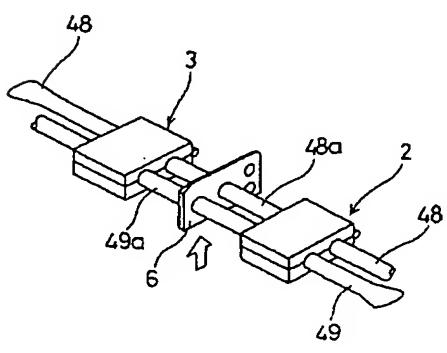
【図 2 0】



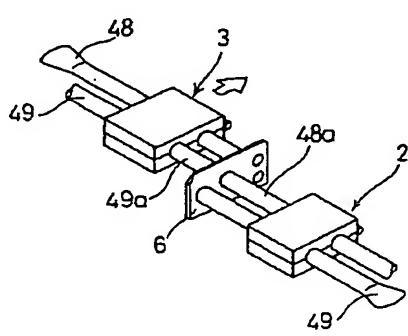
【図 3】



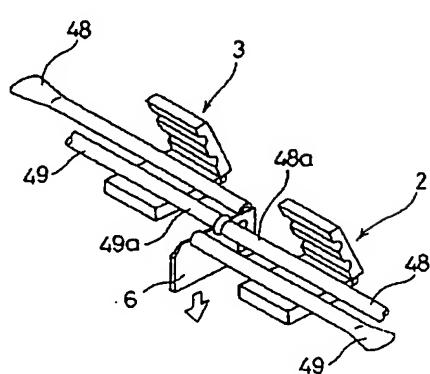
【図 16】



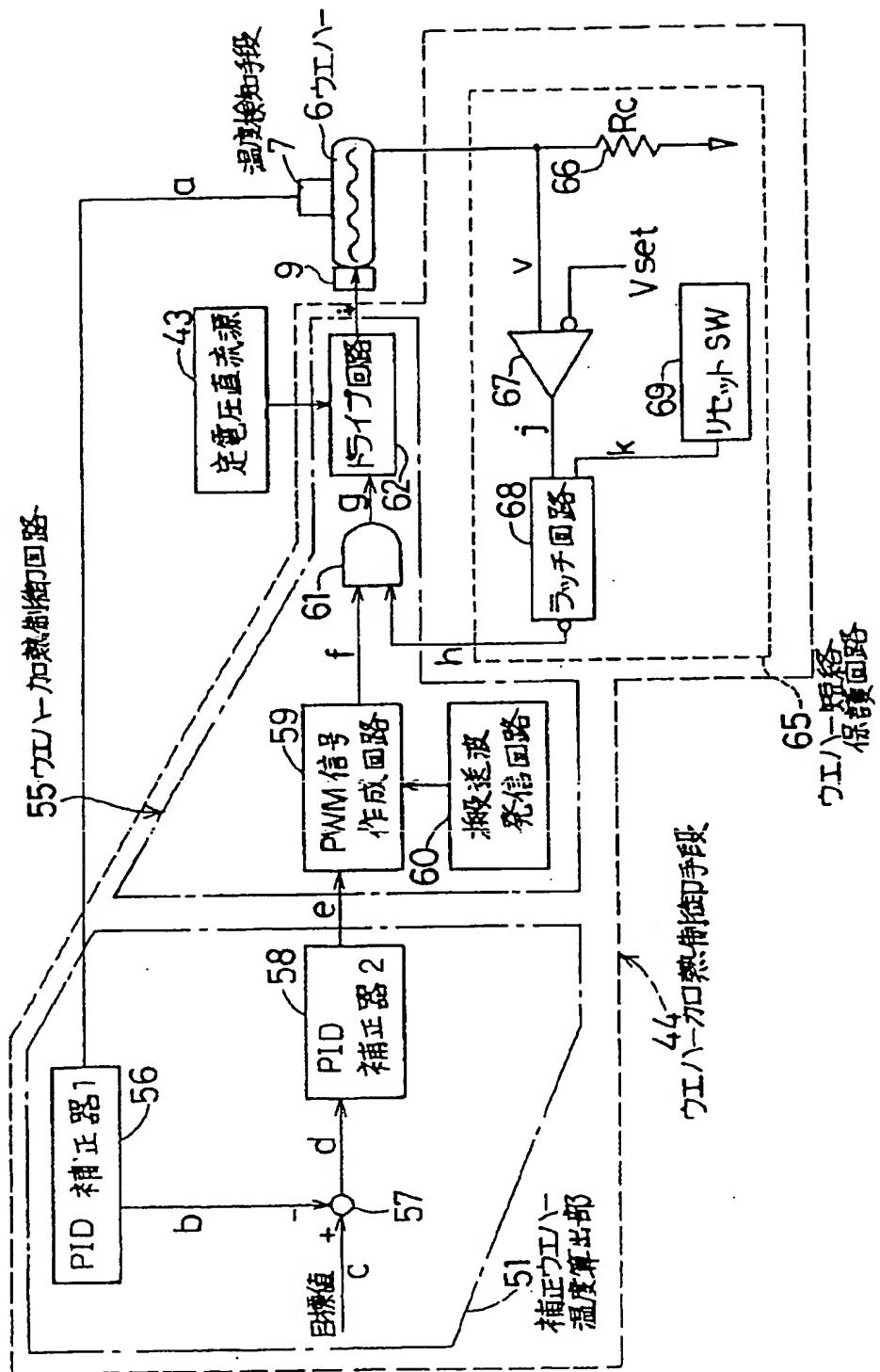
【図 17】



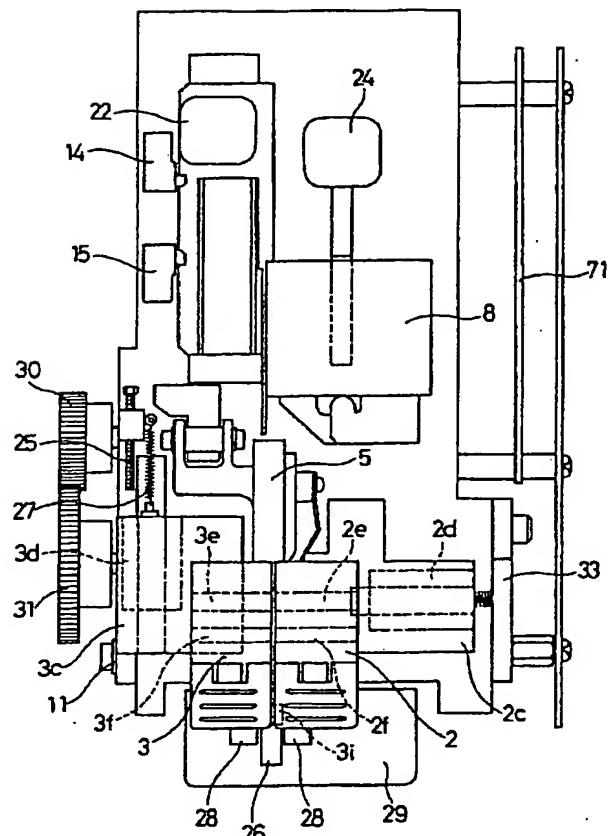
【図 18】



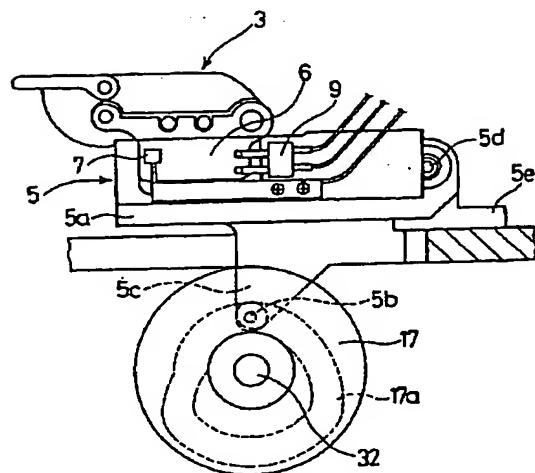
【図 4】



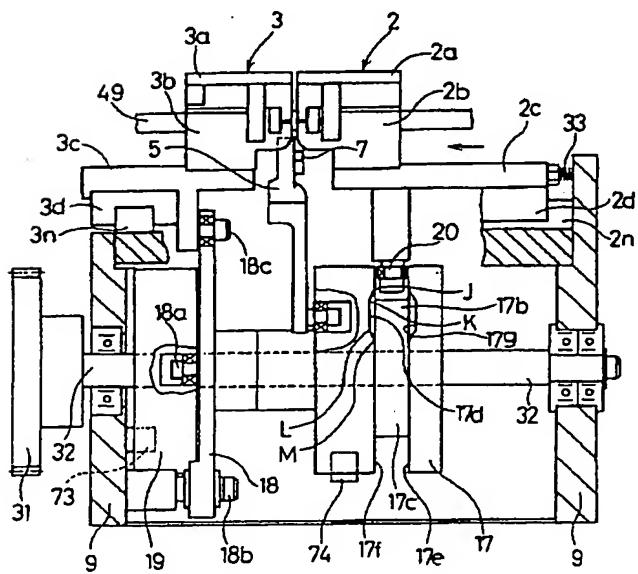
[図5]



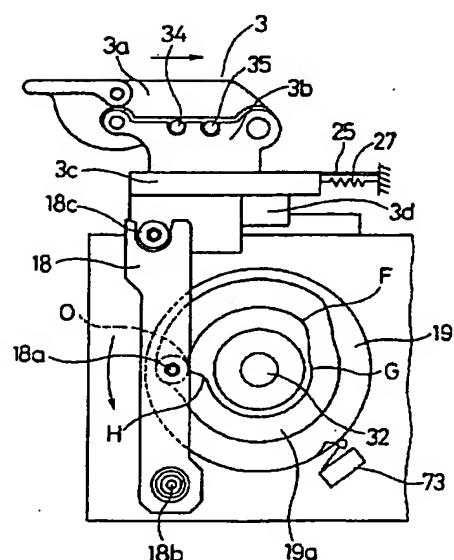
[图 6]



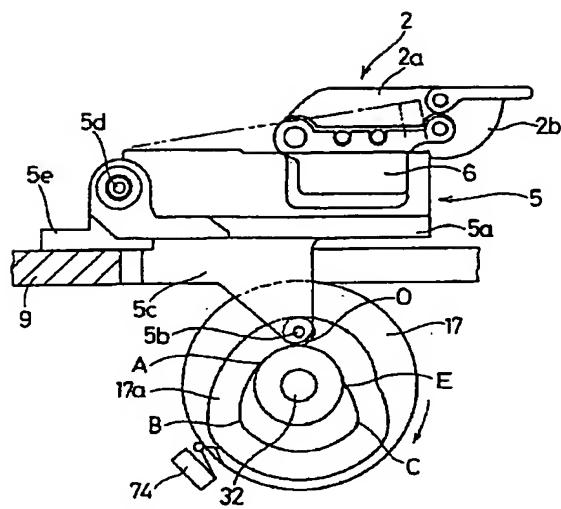
( 7)



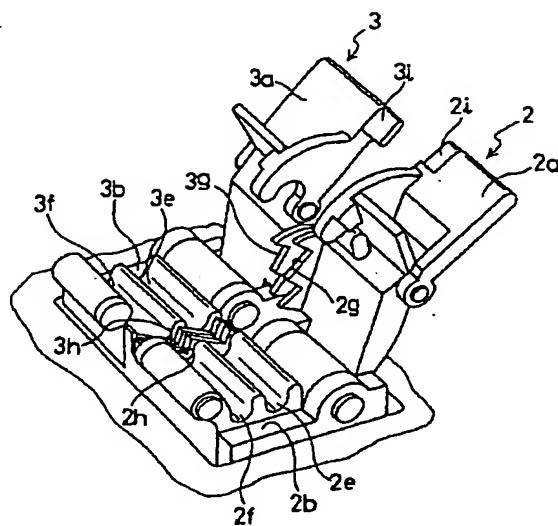
(图 8)



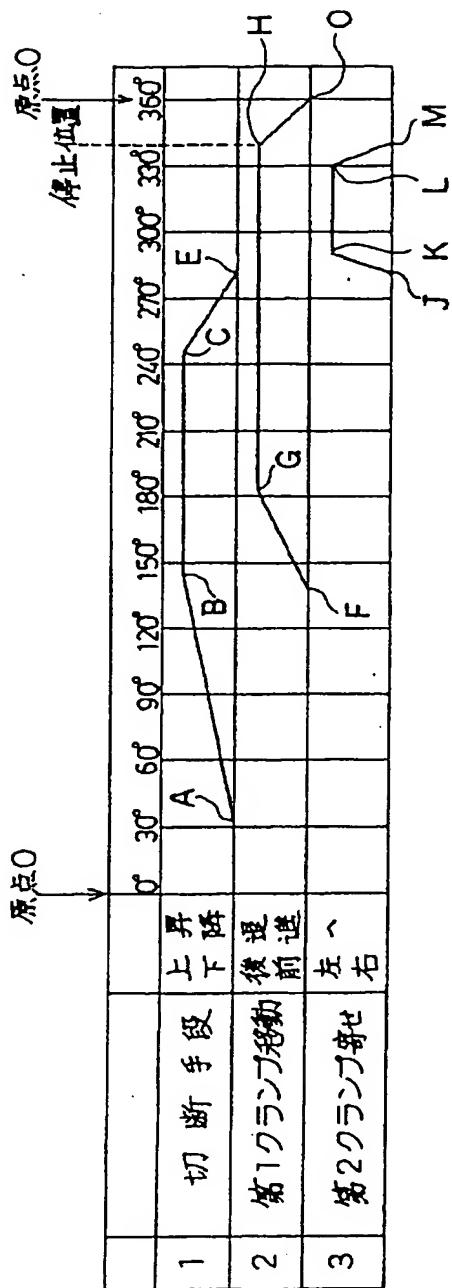
【図 9】



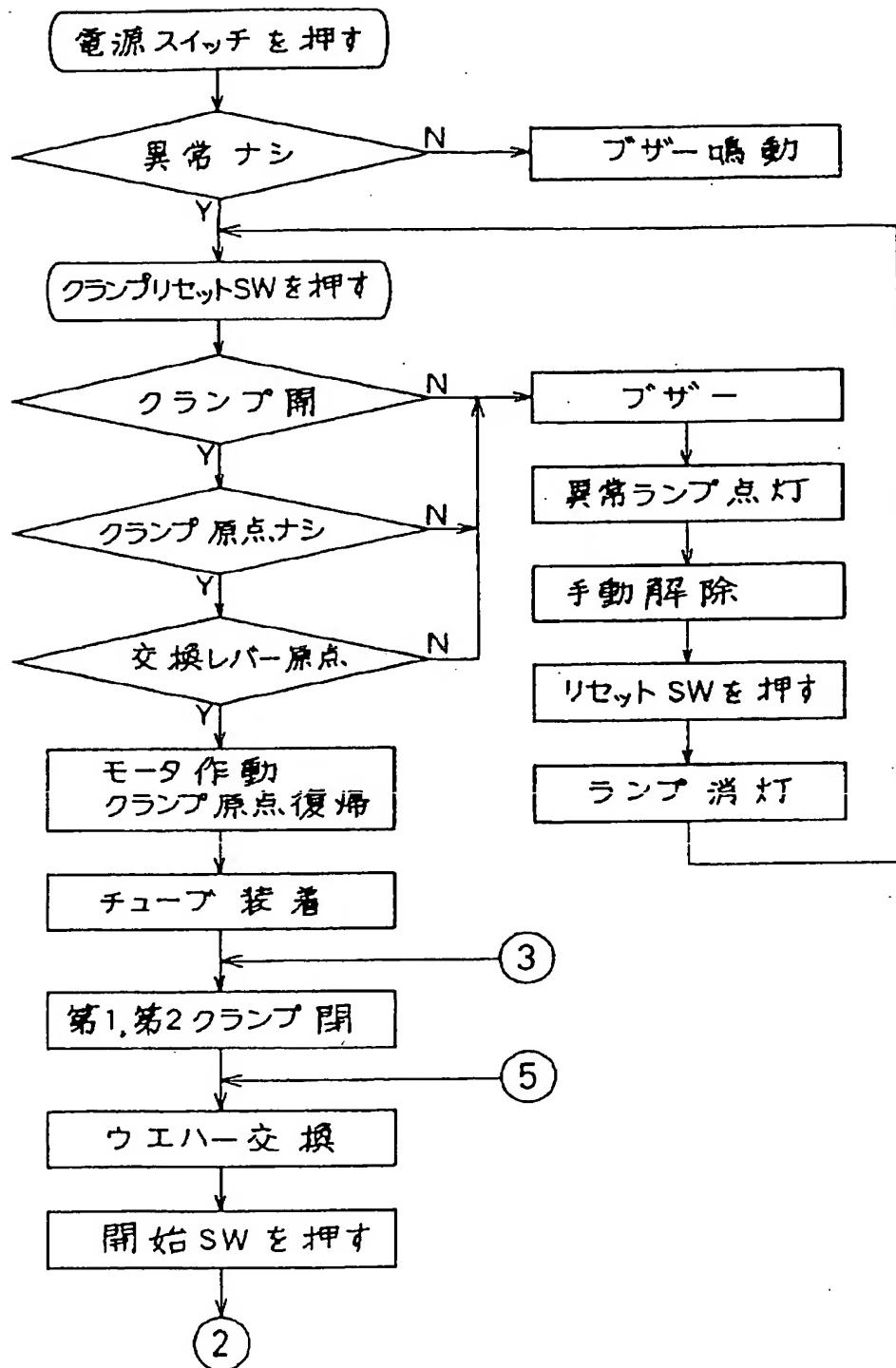
【図 10】



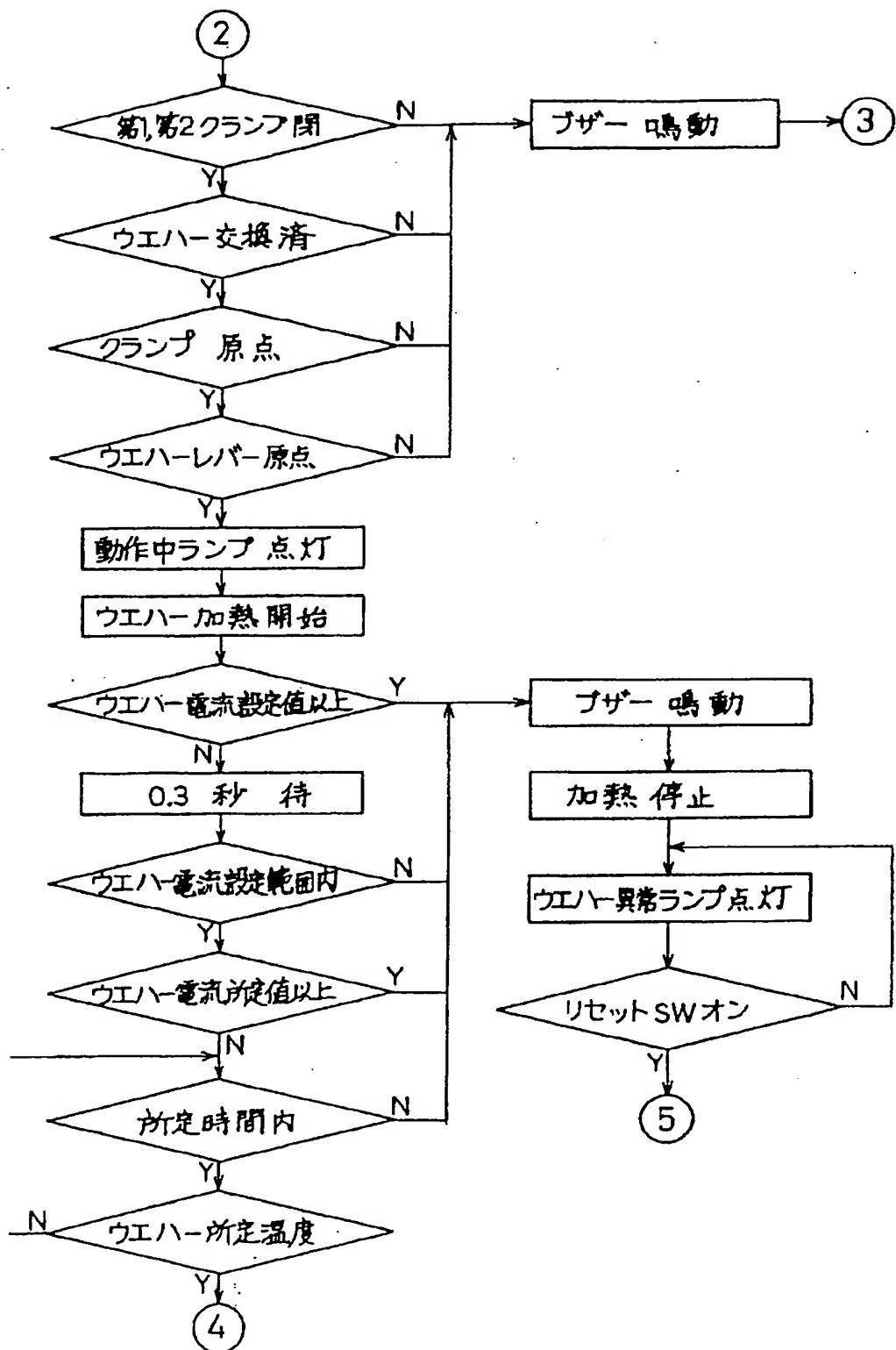
【図11】



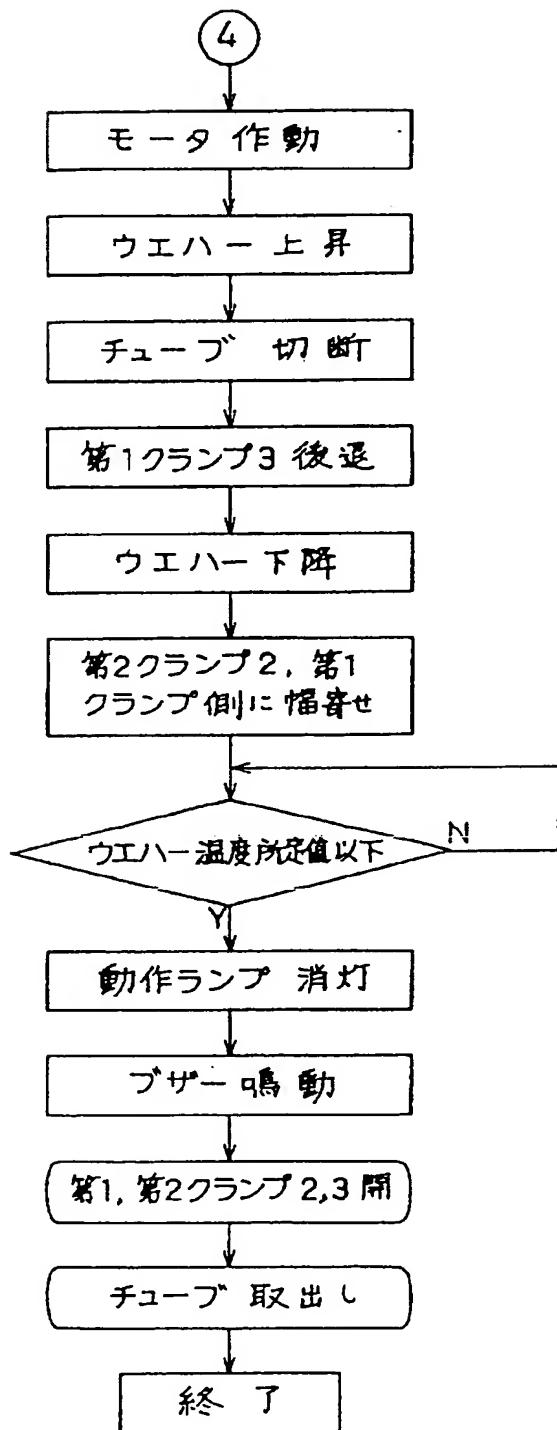
【図 12】



【図13】



【図 14】



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